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Liquid bridge length scale based nondimensional groups for mapping transitions between regimes in capillary break-up experiments

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Criteria to identify transitions between dynamic self-similar linear thinning regimes of liquid bridges are of utmost importance in order to accurately interpret results in capillary break-up rheometry. Currently available criteria encompass many experimental difficulties or rely on numerical approaches. Here, we introduce a different set of nondimensional groups, $Oh_L = \eta_{in}/\sqrt{\gamma\rho L}$ and $a = R/L$, based on the experimentally relevant axial length scale of a liquid bridge L , for viscous-dominated fluids undergoing capillary break-up in air. This framework is further extended to encompass the effect of outer viscous fluids. As a result, we present a two-dimensional operating map in which the boundaries are set by fluid properties and a single geometrical parameter, related to the experimental configuration. This approach establishes guidelines to correctly interpret experimental data and identify transitions in capillary break-up experiments of liquid bridges surrounded by fluids of different viscosities.

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Capillary break-up has been extensively employed in the past as a tool to study the thinning behavior of complex fluid bridges and to extract material properties in extensional flows such as the transient (apparent) extensional viscosity, or the longest relaxation time [1,2]. Nonetheless, a successful application of this technique relies on a proper identification of the underlying dynamics, originating either from a balance or dominance of single material properties that causes the minimum liquid bridge radius R_{min} to exhibit a certain scaling $R_{min} = Hf(t)$, with $f(t)$ some function of time t . In most cases, similarity solutions were needed to determine the necessary numerical prefactors H for a quantitative evaluation of a scaling regime [3]. A multitude of dynamical regimes and $f(t)$, such as viscocapillary (V) [4], elastocapillary (EC) [5], inertia capillary (IC) [6,7], and inertia viscous (IV) [8], have been identified in the literature based on the relevant force balance. Additional regimes were highlighted in more complex scenarios, for instance, when the viscosity of the surrounding fluid cannot be neglected [two-fluid viscous (LV) and line-sink flow (LSF) regimes [9,10]], for bubbles undergoing capillary thinning in fluids of various viscosities [11] or for confined flows [12]. A comprehensive description can be found in Refs. [1,13,14].

Intensive theoretical studies, usually based on scaling arguments, were carried out to formulate criteria that allow one to identify the presence of these regimes and their transitions [13,15]. This

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41 is in particular necessary for regimes that exhibit the same $f(t)$ [as the linear V, IV, and LV
 42 (LSF) regimes], so that an experimentally observed scaling is not sufficient for their identification.
 43 However, Eggers and Villermaux [13] address that discrepancies exist between proposed criteria
 44 for V to IV transitions and experimental observations [16,17], possibly depending on the overall
 45 geometry, which can also be seen in Ref. [18]. One cause lies in limitations to access criteria
 46 that focus on the thinning stages close to break-up, hence close to or below (optical) resolution
 47 limits. Second, effective criteria based on local velocities, local gradients, or Reynolds numbers [19]
 48 require information that is hardly experimentally available and rely on numerical calculations.
 49 Third, and most important, the experimental axial length scales of the liquid bridge have so far
 50 not been taken into account. Although case-specific geometrical parameters were employed to
 51 determine global behavior and regime transitions, they are usually buried in prefactors and arbitrary
 52 constants.

53 The purpose of this Rapid Communication is therefore to establish a systematic framework to
 54 identify transition criteria between linear thinning regimes in liquid bridges, solely based on material
 55 properties and characteristic dimensions of different experimental setups. To this end, we introduce
 56 a set of nondimensional groups based on the experimentally relevant axial length scale of the liquid
 57 bridge. The concept of an axial Ohnesorge number Oh_L , along with the nondimensional radius a ,
 58 is initially introduced for Newtonian, viscous-dominated fluids undergoing capillary break-up in
 59 air. Subsequently, the analysis is extended to encompass the effect of outer fluids of significant
 60 viscosity. Experimental limits, which depend on the setup configuration, are employed to identify
 61 the observable regimes and their transitions. As a result, a two-dimensional (2D) operating map,
 62 in which the boundaries are set by our dimensionless groups and the dependent scaling relations,
 63 is introduced. This map is an alternative guideline to identify regimes and interpret experimental
 64 observations for viscous liquids surrounded by air and fluids of different viscosities.

65 For Newtonian fluids, the balance controlling the radial thinning behavior has been given in
 66 terms of the global Ohnesorge number $Oh = \eta_{in}/\sqrt{\gamma\rho R}$ that compares radial viscous and inertial
 67 contributions (where η_{in} is the shear viscosity, γ the surface tension, ρ the density, and R the
 68 characteristic radial dimension of the liquid bridge). For a viscous-dominated thinning (V regime),
 69 Papageorgiou [4] exploited a similarity solution to show that the prefactor in the linear decay of the
 70 minimum radius of a slender liquid bridge $R_{min} \sim -H\gamma t/\eta_{in}$ takes on the value $H = 0.0709$ [20].
 71 As the liquid bridge thins, inertia becomes progressively more significant [21], leading eventually
 72 to a transition to the also linear inertia-viscous regime (IV), for which $H = 0.0304$ [8]. However,
 73 as indicated above, a transition criterion between the V and IV regime that scales with Oh [13]
 74 deviates up to orders of magnitude for different experimental setups. We propose that the underlying
 75 difference between the experiments is the length L of the liquid bridge, which is so far missing in
 76 the dimensional analysis. Including an axial length scale L , it is straightforward to show that the
 77 Buckingham Π theorem yields as one possible solution for the now two alternative groups

$$Oh_L = \frac{\eta_{in}}{\sqrt{\gamma\rho L}}, \quad a = \frac{R}{L}, \quad (1)$$

78 and thus as a transition criterion, $Oh_L^2 a$ that can also be derived balancing axial inertial and
 79 viscous stresses. Both groups now incorporate with the axial length scale L an unconventional
 80 nondimensionalization of the fluid properties that captures, however, the essential geometrical
 81 differences between experimental setups, which was generally not possible with the traditional
 82 nondimensionalization using an often arbitrary initial radial length R . In the most commonly used
 83 capillary break-up techniques, the liquid bridge is held between two fixed boundaries: in capillary
 84 break-up extensional rheometry (CaBER) experiments [20] between circular plates, with adjustable
 85 distances of $O(1 \text{ cm})$, in a Rayleigh-Ohnesorge jetting extensional rheometer (ROJER) [22]
 86 between equidistant [$O(100 \mu\text{m})$] droplets on a flying jet, while dripping-onto-substrate extensional
 87 rheometry (DOS) [23] probes a liquid bridge of $O(1 \text{ mm})$ confined between a nozzle and a
 88 substrate. Contrary to unconfined liquid *filaments*, extensively studied by Schulkes, Basaran,

and Hutchings [24–27], the liquid *bridge* length (and thus L) is fixed for a capillary break-up experiment [13], but differs up to two orders of magnitude between the different configurations.

The significance of the axial length scale is supported by a transition criterion between the V and IV regime recently introduced by Li and Sprittles [28], which they suggested to take place when the local Reynolds number $Re = \rho u L / \eta_{in}$ (where u is the local axial velocity at an axial distance L away from the point of minimal axial velocity) reaches at the point of maximum axial velocity u_{max} (at L_{max}) a critical value of $Re = 0.85$. One can decouple Re (and conveniently avoid the experimentally difficult to access local velocity) into Oh_L and a by approximating the slender liquid bridge with a cylindrical geometry. Replacing in Re the axial velocity via the strain rate $\dot{\epsilon} = u/L = -2\dot{R}/R$, using the linear radius decay of Papageorgiou for viscous fluids [4], yields $Re = (2H\rho\gamma L^2)/(\eta_{in}^2 R) = 0.1418/(Oh_L^2 a)$.

V to IV. We can now determine the critical transition criteria for the dimensionless radius a exclusively based on fluid properties using the axial Oh_L of Eq. (1), once the critical liquid bridge length scale L is introduced. Without recurring to numerical methods, a critical axial length scale L , defined as the axial distance L_{max} between the point of maximum and zero axial velocity (analogously to Ref. [28]), can be accessed from the velocity profiles derived from the experimentally obtained liquid bridge shapes. In the V regime, this L_{max} is predicted to scale with time only as $\sim (t_b - t)^{0.175}$ [3,4], and this near time independence has been numerically [28] and experimentally (see the Appendix) confirmed. Using the numerically determined transition criterion of $Re = 0.85$ [28] would give $(Oh_L^2 a)_{crit} = 0.17$. However, taking into account the experimentally observed deviations from the ideal cylindrical shape via an experimentally observed correction factor of 1.5 (see the Appendix) gives for the transition from V to IV,

$$a_{crit} = \frac{R_{crit}}{L} = \frac{0.11}{Oh_L^2}. \quad (2)$$

V to LV. Next, we apply this alternative nondimensionalization via L to identify the transitional criteria also in the presence of an outer immiscible fluid of significant viscosity, assuming the inner fluid to be incompressible and the density mismatch between the two fluids $\Delta\rho$ insignificant [29,30]. Lister and Stone [9] have shown that, even for low viscous outer fluids, the drag exerted by the outer liquid can no longer be neglected when break-up is approached. Introducing the nondimensional viscosity ratio $p = \eta_{in}/\eta_{out}$ of inner to outer fluid, for $p \gg 1$ the flow inside the liquid bridge is predominantly a uniaxial extension and causes a radially decaying shear drag on the outer fluid [see Fig. 1(a)]. They approximated this drag as the shear stress induced by a cylinder sliding axially through the outer fluid, yielding the momentum balance [in terms of a of Eq. (1)],

$$\frac{\gamma}{R} = 3p\eta_{out}\dot{\epsilon} - \frac{B\eta_{out}}{2a^2}\dot{\epsilon}, \quad (3)$$

where $B = 2/|\ln a|$ is a dimensionless coefficient [9]. The dimensionless group that arises when balancing inner and outer fluid stresses on the right-hand side of Eq. (3) is $pa^2|\ln a|$, which describes the transition from the V regime, where viscous stresses generated by the outer fluid are negligible, to one in which they control the thinning behavior (LV). Again, we can describe the transition in terms of a critical radius,

$$a_{crit}^2 |\ln a_{crit}| = \frac{1}{3p}. \quad (4)$$

LSF to LV. As pointed out by Sierou and Lister [10], a drastically different physical picture is seen for small viscosity ratios ($p \ll 1$). In the outer fluid, the flow is a nearly pure radial extension, resembling a line distribution of sinks, while a parabolic shear (Poiseuille) flow occurs in the inner liquid, as illustrated in Fig. 1(a). The momentum balance takes on the form

$$\frac{\gamma}{R} = \frac{4u\eta_{out}L}{R^2} + \eta_{out}\frac{u}{L}, \quad (5)$$

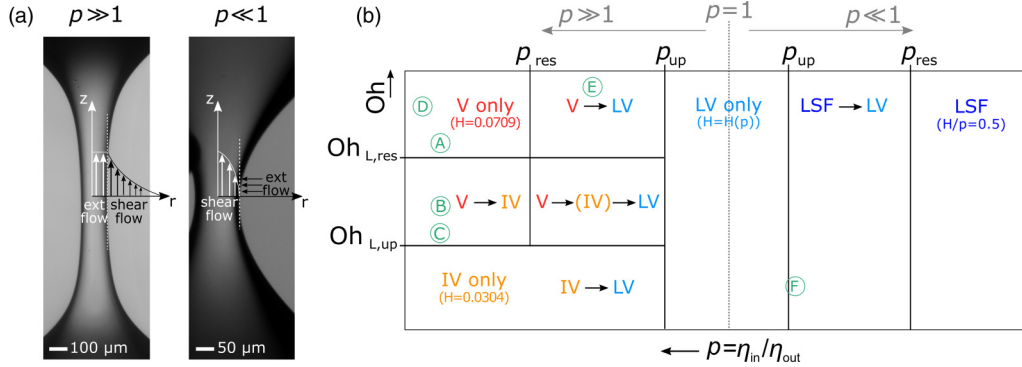
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FIG. 1. (a) High-resolution images from CaBER experiments performed with a surrounding immiscible outer liquid ($p^{\gg 1} = 18.7$ and $p^{\ll 1} = 0.002$). The schematics highlights the differences in the expected inner and outer flow profiles for $p \gg 1$ and $p \ll 1$, respectively. (b) 2D operating map as a function of the dimensionless groups Oh_L and p . The derived criteria are used to delimit the areas within which specific regimes and transitions can be experimentally detected. Circled green letters corresponds to the capillary break-up experiments for various L , and inner and outer fluid viscosities of Fig. 2.

129 in which u is the radially averaged velocity in the axial direction in the inner fluid. Balancing the two
 130 terms on the right-hand side in Eq. (5) establishes the transition from a thinning regime dominated
 131 by the radial drag of the outer fluid [line-sink flow (LSF)] to the point where viscous friction of
 132 the inner fluid can no longer be neglected (LV), and determines a dimensionless group p/a^2 . The
 133 critical transition criterion can then be rewritten as

$$a_{crit} = \sqrt{4p}. \quad (6)$$

134 *Observation limits for transitions.* The transitional criteria for a introduced above are defined
 135 solely based on material properties and one geometrical parameter via the dimensionless groups Oh_L
 136 and p . It is crucial to note that an a_{crit} can vary significantly for the same fluid due to the intrinsically
 137 different axial dimensions and length scales L employed in the various capillary break-up techniques
 138 CaBER [20], DOS [23], and ROJER [22]. This also entails that the same regimes and transitions
 139 might not necessarily be observable in capillary break-up experiments performed on the same fluid,
 140 but with different techniques (and thus different L). However, since L is observed to not change
 141 significantly in time in the V regime, this geometry-dependent length scale can be used to assess the
 142 observation range for different setups. The derived transitional criteria can be reworked as

$$Oh_L = \sqrt{\frac{0.11}{a_{crit}}}, \quad p^{\gg 1} = \frac{|\ln(a_{crit})|^{-1}}{3a_{crit}^2}, \quad p^{\ll 1} = \frac{a_{crit}^2}{4}. \quad (7)$$

143 Setting a_{crit} equal to the upper and lower observation limits of the radius for a given L of a setup
 144 allows us to determine *a priori* for which Oh_L , $p^{\gg 1}$, or $p^{\ll 1}$ an a_{crit} can be experimentally observed.
 145 Since most regimes are based on a slenderness assumption (i.e., $a = R/L \ll 1$), a first limit is set
 146 by an upper radius R_{up} , so that $a_{crit} \leq a_{up} = R_{up}/L$ in order for a transition to be observable. Using
 147 Eq. (7), a_{up} identifies then the critical global $Oh_{L,up}$ below which no transition but only the IV regime
 148 is observed. Similarly, the upper slenderness limit a_{up} can also be used to determine the viscosity
 149 ratio $p_{up}^{\gg 1}$ below which only the LV regime is visible for a set L . An upper criterion for $p \ll 1$
 150 can, however, not be derived based on the same argument in a straightforward fashion. Due to the
 151 quadratic nature of the liquid bridge profile in the LSF regime [32], L is much smaller compared to
 152 the other cases [see, for example, the image for $p \ll 1$ in Fig. 1(a)] and the bridge only becomes
 153 sufficiently slender when the transition to LV itself takes place. Nonetheless, a slenderness-based

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limit $p_{\text{up}}^{\ll 1}$ can still be used to determine the critical viscosity ratio below which the LSF regime can be detected right before transitioning to the slender LV regime.

The lower critical boundary is set by the radial resolution limit R_{res} , which varies significantly with the experimental detection technique [11] and is usually disregarded in numerical studies. As for the upper limit, from $a_{\text{crit}} \geq a_{\text{res}} = R_{\text{res}}/L$, the lower limits $\text{Oh}_{\text{L,res}}^{\gg 1}$, $p_{\text{res}}^{\gg 1}$, and $p_{\text{res}}^{\ll 1}$ are obtained from Eq. (7).

All the aforementioned limits are illustrated in Fig. 1(b) where a 2D map describes the observable regimes and transitions in terms of Oh_{L} and p and thus the respective radii (once the fluid properties and in particular the axial length L of the setup are known).

Experimental verification. To verify our introduced criteria and limits, we use the map in Fig. 1(b) to predict the behavior and transitions for a number of experiments encompassing the 2D parameter space. The capillary break-up experiments are performed using a CaBER rheometer (Thermo Haake, high-speed video-imaging re-equipped). a_{up} is calculated assuming a slenderness limit $L/R = 10$ [28], and a_{res} is calculated based on the limit of the optical setup, which can accurately resolve down to a radius of $5 \mu\text{m}$. The geometrical parameter L is determined following the Appendix, and is experimentally found to be directly related to the final plate separation distance. Water and glycerol-water mixtures are used as inner fluids, and air and silicon oils of different viscosities as outer fluids.

To show the importance of the geometry to determine the onset of the V to IV transition, in a first series of experiments [A, B, and C in Fig. 1(b)] we move through the map down the vertical axis for a high, fixed value of p . The experiments are performed with the same inner fluid ($\eta_{\text{in}} = 0.365 \text{ Pa s}$, $\gamma = 65 \text{ mN m}$) surrounded by air ($p = 24\,333$), while the geometrical factor L is changed by varying the final plate distance. The temporal evolution of the minimum radius is shown in Fig. 2(a) for the three cases, together with the thinning predictions for the V regime ($H = 0.0709$) and the IV regime ($H = 0.0304$). Figure 2(a) clearly illustrates how the window between R_{up} and R_{crit} for the observation of a transition, drastically increases by increasing L . Moreover, R_{crit} markedly corresponds to the radius at which experimental data start deviating from the theoretical V thinning, thus accurately predicting the onset of a transition to IV. A second series of experiments [D and E in Fig. 1(b)] shows the effect of increasing viscosity of the outer fluid while keeping L and inner fluid properties constant ($\eta_{\text{in}} = 0.518 \text{ Pa s}$). With air as the outer fluid, case D ($p = 34\,435$) is comparable to case A, where the transition to IV is below the resolution limit, as shown by the minimum radius evolution in Fig. 2(b). By adding an outer liquid of sufficiently high viscosity ($p = 96$), R_{crit} calculated with Eq. (4) lies now within the experimentally detectable range and nicely corresponds to the experimentally observed onset of the LV regime in Fig. 2(ii). Moving to the other side of the map towards low viscosity ratios, case F in Fig. 1(ii) ($\eta_{\text{in}} = 10^{-3} \text{ Pa s}$, $p = 0.002$) represents an area of the map at the limits of experimental accessibility. Nonetheless, the R_{min} evolution in Fig. 2(c) shows that Eq. (6) precisely predicts the transition from LSF to LV.

To conclude, in this Rapid Communication, we introduce a theoretical framework for capillary break-up experiments to determine the critical transition radii between dynamical regimes when viscous stresses are governing the inner or outer fluid flows (or both). Our criteria depend solely on fluid properties via an alternative set of nondimensional groups incorporating the axial length scale L of the liquid bridge, which is for slender filaments in the V regime directly related to the axial dimension of the experimental setup. The criteria describe a 2D map to be used as a guideline to correctly pinpoint the observability of transitions between linear thinning regimes in experiments, as proven by examples covering a wide parameter range. Still, further experiments are needed to refine the inner part of the parameter space. In particular, the IV to LV transition is indicated to take place at $a \sim p^{-1/2}$ [9], but the correlation of the length scale L to the geometrical parameters of the bridge in the IV regime is unexplored. A full comprehension of predominantly viscous fluids will allow us to expand the map to more difficult scenarios, including the presence of viscoelasticity, for which the operating space could be expanded to 3D by introducing the Deborah (De) or Weissenberg (Wi) numbers.

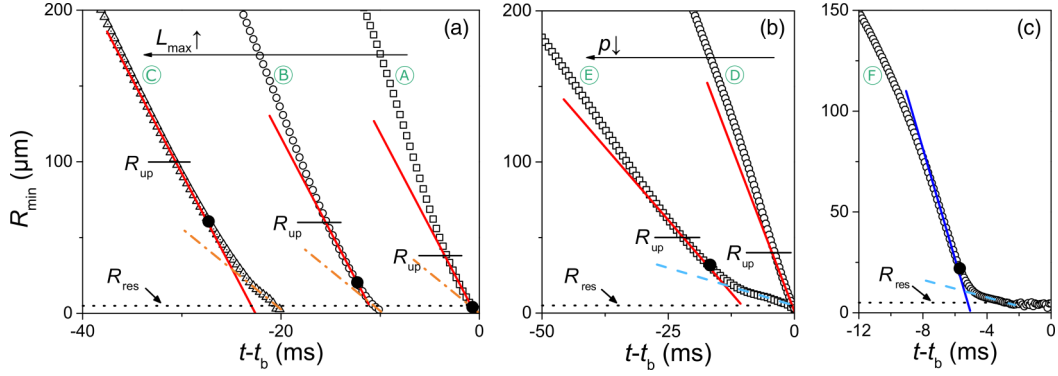
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FIG. 2. Minimum radius evolution (R_{\min}) in time, with t_b as the break-up time, for several fluids and geometrical conditions in CaBER experiments performed in air [(a), (b) (open circles)] and with an outer liquid [(b) (open squares), (c)]. Solid dots represent calculated R_{crit} . Thinning curves in A are shifted 10 ms apart for clarity. (a) Experimentally detectable regimes are determined by the set geometrical conditions. For the same fluid ($\eta_{\text{in}} = 0.365$ Pa s, $\gamma = 65$ mN m), R_{crit} via Eq. (2) shifts to larger radii and the experimental window ($R_{\text{up}} - R_{\text{res}}$) expands as the geometrical parameter L increases (right to left: 480, 600, and 1000 μm). Consistently, the thinning dynamics appear to be solely V dominated for the lowest L (open squares), whereas a region following the IV scaling is clearly distinguishable for the highest L (open triangles). R_{crit} predicted with Eq. (2) matches the deviation of the data from the predicted V scaling ($H = 0.0709$, red solid line) towards the IV scaling ($H = 0.0304$, orange dashed-dotted line). (b) Thinning curves of the same inner fluid ($\eta_{\text{in}} = 0.518$ Pa s, $\gamma = 63.7$ mN m and 30.0 mN m for D and E, respectively) at comparable geometrical conditions show different behaviours depending on the outer medium viscosity. For $p \gg 1$, the transition from V ($H = 0.0709$, red solid line) to LV regime [$H(p) = 0.02$ [31], blue dashed line] is detectable only if η_{out} is sufficiently high to fulfill the condition $p_{\text{res}} \ll p \ll p_{\text{up}}$ (open circles $p = 34435$, open squares $p = 96$). (c) For $p = 0.002$, R_{crit} according to Eq. (4) correspond to the deviation from LSF ($H = 0.5$, blue solid line) to the LV regime [$H(p) = 0.04$ [10], blue dashed line].

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APPENDIX

206 To decouple Re into Oh_L and a , the liquid bridge was approximated as a perfect cylinder for
 207 which the axial velocity $u = \dot{L}$ increases linearly along the bridge axis. Nonetheless, actual fluid
 208 bridges exhibit an axial curvature [Fig. 3(a)], which causes a significant deviation of $u(z)$ from
 209 linearity. Here, we introduce an experimental method to determine the radially averaged axial
 210 velocity $u_a(z, t)$, a numerical correction factor C accounting for this deviation for the determination
 211 of a_{crit} [Eq. (2)], and the length L_{max} at $u_{a,\text{max}}$.

212 $u_a(z, t)$ [Fig. 3(b)] can directly be obtained from the experimentally observed evolution of
 213 the bridge shape, following the approach of Rothert *et al.* [16]. For this the cumulative volume
 214 $V_{\text{cumul}}(z = z_0 + i\Delta z, t) = \sum_{z_0}^{z_0+i\Delta z} \Delta z \pi R^2(z_0 + i\Delta z, t)$ is determined from the radius evolution
 215 [with $z_0(t)$ the position of the minimum radius and Δz the pixel size]. Assuming zero axial velocity
 216 at $z_0(t)$, the axial velocity at position z is

$$u_a(z, t) = \frac{1}{\pi R^2(z, t)} \frac{dV_{\text{cumul}}(z, t)}{dt}. \quad (\text{A1})$$

217 Due to axial curvature at the bridge end bulges, the actual average axial velocity profile exhibits a
 218 sinusoidal shape [Fig. 3(b)], allowing us to determine a u_{max} at L_{max} . Plotting $L_{\text{max}}(t)$ in Fig. 3(c)
 219 shows that, within the V regimes, L_{max} remains approximately constant for different experimental
 220 conditions of Fig. 2. The inset in Fig. 3(b) shows the overestimation of the velocity at $z = L_{\text{max}}$
 221 when assuming a linear increase of u with z . Evidently, also the calculated R_{crit} in Fig. 3 (solid dot,
 222 calculated from $a_{\text{crit}} = R_{\text{crit}}/L_{\text{max}} = 0.17 \text{ Oh}_L^2$) lies then above the actual transition radius compared

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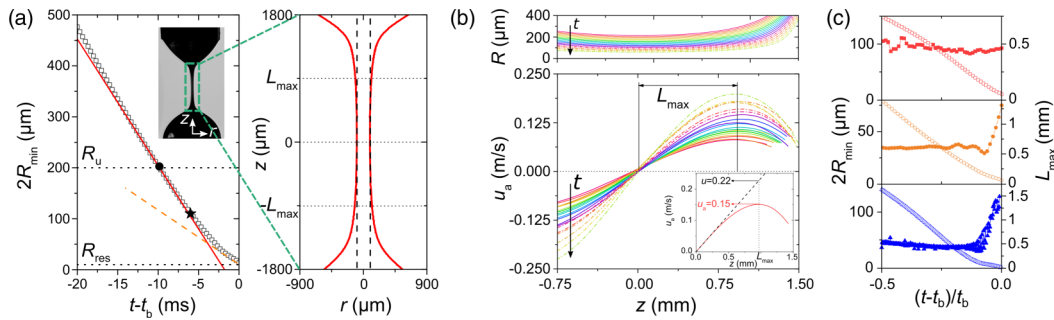


FIG. 3. (a) Capillary thinning evolution of a Newtonian fluid with $\eta_{in} = 0.365$ mPa s in air and with $L_{max} = 900$ μm . R_{crit} calculated from the linear evolution of u (black solid dot, high-resolution image in the inset) overestimates the V to IV transition, which is instead correctly captured by R_{crit} calculated incorporating the corrective factor C in Eq. (2) (black solid star). The enlargement of the inset shows the visible difference between the ideal cylinder geometry (black dashed lines) and the actual profile (red solid lines). (b) Temporal evolution of $R(z)$ and $u_a(z)$ in a capillary break-up experiment of a glycerol-water mixture in air ($\eta_{in} = 0.365$ mPa s) with $L_{max} = 900$ μm (-18.33 ms $< t - t_b < -6.33$ ms at $\Delta t = 0.66$ ms). Inset: The deviation of the real profile from the ideal cylinder geometry implicates the large difference at L_{max} between $u_a = 0.15$ m/s (red solid line) and $u = 0.22$ m/s (black dashed line) calculated assuming a linear evolution of the axial velocity. (c) Direct comparison between the temporal evolution of R_{min} (open symbols) and L_{max} (solid symbols), determined from the experimental u_a profiles. The characteristic length remains approximately constant throughout the complete bridge evolution for case A of Fig. 2 (top, red squares). Also for cases B (middle, orange circles) and E (bottom, blue triangles) L_{max} remains constant in the V regime, up to the transitions to the asymmetrical thinning regimes (IV or LV).

to experimental data, while the theoretical V and IV scalings (red solid and orange dashed lines, respectively) suggest a much later transition. To correct for this overestimation, $C = u_{act}/u$ at L_{max} has been calculated for several CaBER experiments performed on V-dominated fluids at different L . Remarkably, C assumes a constant value of 1.5, and is used to quantitatively correct the criterion derived for a_{crit} [Eq. (6)]. The corrected R_{crit} [Fig. 3(a), black solid star] corresponds then to the deviation from the V scaling, indicating the transition to the IV regime.

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