

1 **BINDERS ALTERNATIVE TO PORTLAND CEMENT AND WASTE MANAGEMENT FOR**  
2 **SUSTAINABLE CONSTRUCTION – Part 2**

3 Luigi Coppola<sup>1</sup>, Tiziano Bellezze<sup>2</sup>, Alberto Belli<sup>2</sup>, Maria Chiara Bignozzi<sup>3</sup>, Fabio Bolzoni<sup>4</sup>,  
4 Andrea Brenna<sup>4</sup>, Marina Cabrini<sup>1</sup>, Sebastiano Candamano<sup>5</sup>, Marta Cappai<sup>6</sup>, Domenico  
5 Caputo<sup>7</sup>, Maddalena Carsana<sup>4</sup>, Ludovica Casnedi<sup>6</sup>, Raffaele Cioffi<sup>8</sup>, Ombretta Cocco<sup>6</sup>,  
6 Denny Coffetti<sup>1</sup>, Francesco Colangelo<sup>8</sup>, Bartolomeo Coppola<sup>9</sup>, Valeria Corinaldesi<sup>2</sup>,  
7 Fortunato Crea<sup>5</sup>, Elena Crotti<sup>1</sup>, Valeria Daniele<sup>10</sup>, Sabino De Gisi<sup>11</sup>, Francesco Delogu<sup>6</sup>,  
8 Maria Vittoria Diamanti<sup>4</sup>, Luciano Di Maio<sup>9</sup>, Rosa Di Mundo<sup>11</sup>, Luca Di Palma<sup>12</sup>, Jacopo  
9 Donnini<sup>2</sup>, Ilenia Farina<sup>8</sup>, Claudio Ferone<sup>8</sup>, Patrizia Frontera<sup>13</sup>, Matteo Gastaldi<sup>4</sup>, Chiara  
10 Giosuè<sup>2</sup>, Loredana Incarnato<sup>9</sup>, Barbara Liguori<sup>7</sup>, Federica Lollini<sup>4</sup>, Sergio Lorenzi<sup>1</sup>, Stefania  
11 Manzi<sup>3</sup>, Ottavio Marino<sup>7</sup>, Milena Marroccoli<sup>14</sup>, Maria Cristina Mascolo<sup>15</sup>, Letterio Mavilia<sup>16</sup>,  
12 Alida Mazzoli<sup>2</sup>, Franco Medici<sup>12</sup>, Paola Meloni<sup>6</sup>, Glauco Merlonetti<sup>2</sup>, Alessandra Mobili<sup>2</sup>,  
13 Michele Notarnicola<sup>11</sup>, Marco Ormellese<sup>4</sup>, Tommaso Pastore<sup>1</sup>, Maria Pia Peddeferri<sup>4</sup>, Andrea  
14 Petrella<sup>11</sup>, Giorgio Pia<sup>6</sup>, Elena Redaelli<sup>4</sup>, Giuseppina Roviello<sup>8</sup>, Paola Scarfato<sup>9</sup>, Giancarlo  
15 Scoccia<sup>10</sup>, Giuliana Taglieri<sup>10</sup>, Antonio Telesca<sup>14</sup>, Francesca Tittarelli<sup>2</sup>, Francesco Todaro<sup>11</sup>,  
16 Giorgio Vilardi<sup>12</sup>, Fan Yang<sup>4</sup>  
17

18 <sup>1</sup> Department of Engineering and Applied Sciences, University of Bergamo

19 <sup>2</sup> Department of Materials, Environmental Sciences and Urban Planning, Università  
20 Politecnica delle Marche

21 <sup>3</sup> Department of Civil, Chemical, Environmental and Materials Engineering, University of  
22 Bologna

23 <sup>4</sup> Department of Chemistry, Chemical Engineering and Materials “G. Natta”, Politecnico di  
24 Milano

25 <sup>5</sup> Department of Environmental and Chemical Engineering, University of Calabria

26 <sup>6</sup> Department of Mechanical, Chemical and Materials Engineering, University of Cagliari

27 <sup>7</sup> Department of Chemical, Materials and Production Engineering, University of Naples  
28 Federico II

29 <sup>8</sup> Department of Engineering, University of Naples Parthenope

30 <sup>9</sup> Department of Industrial Engineering, University of Salerno

31 <sup>10</sup> Department of Industrial and Information Engineering and Economics, University of  
32 L'Aquila

33 <sup>11</sup> Department of Civil, Environmental, Land, Building Engineering and Chemistry,  
34 Politecnico di Bari

35 <sup>12</sup> Department of Chemical Engineering, Materials and Environment, Sapienza University  
36 of Rome

37 <sup>13</sup> Department of Civil Engineering, Energy, Environment and Materials, Mediterranea  
38 University of Reggio Calabria

39 <sup>14</sup> School of Engineering, University of Basilicata

40 <sup>15</sup> Department of Civil and Mechanical Engineering, University of Cassino and Southern  
41 Lazio

42 <sup>16</sup> Department of Heritage, Architecture and Urban Planning, University of Reggio Calabria  
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## ABSTRACT

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50 The paper represents "a state of the art" on sustainability in construction materials. In Part  
51 1 of the paper, issues related to production, microstructures, chemical nature, engineering  
52 properties and durability of mixtures based on binders alternative to Portland cement were  
53 presented. This second part of the paper concerns use of traditional and innovative Portland-  
54 free lime-based mortars in conservation of cultural heritage and recycling and management  
55 of wastes to reduce consumption of natural resources in production of construction  
56 materials. The latter is one of the main concern in terms of sustainability since nowadays  
57 more the 75% of wastes are disposed in landfills.

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## 59 **1. Introduction**

60 In Part 1 of the paper, issues related to production, microstructures, chemical nature,  
61 engineering properties and durability of mixtures based on binders alternative to Portland  
62 cement were presented. This second part of the paper concerns use of traditional and  
63 innovative Portland-free lime-based mortars in conservation of cultural heritage and  
64 recycling and management of wastes to reduce consumption of natural resources in  
65 production of construction materials. The latter is one of the main concern in terms of  
66 sustainability since nowadays more the 75% of wastes are disposed in landfills.

## 67 **2. Traditional and innovative Portland-free lime based mortar for conservation of** 68 **historical heritage**

### 69 **2.1. Traditional historic mortars**

70 Addition of natural or artificial pozzolans to lime mortars was practiced since the dawn of  
71 civilization. Volcanic eruptions occurred worldwide provided ancient populations with natural  
72 pozzolanic materials (1). In the absence of volcanic materials, man learned to use crushed  
73 bricks or pottery fragments (*cocciopesto* when mixed with lime). Earlier use of pozzolans  
74 has been proven for Galilean archaeological sites dating back to the Neolithic period (2).  
75 Further evidence has been found in Crete and in Greece (2–5). Nevertheless, only in Ancient  
76 Rome pozzolanic materials have undergone systematic exploitation. It is probably during  
77 the century II BC that Romans discover the hydraulic properties of the volcanic ash in the  
78 area near *Puteoli* (6). Hence, the name of *pulvis puteolanus* given to the material, from which  
79 the modern term *pozzolan* derives. Use of such natural aggregate as pozzolanic agent  
80 became constant and rational during the Roman Empire, (7–12). The number of ancient  
81 buildings survived to time and nature injuries well testifies the extraordinary properties of  
82 such Roman mortars (13). Since ancient times, knowledge and expertise have been  
83 summarized by various authors. Vitruvius points out the ability of *harena fossicia* (14,15) of

84 imparting solidity to structures even in water(16,17). Pliny the Elder (*Naturalis Historia*)  
85 confirms the extraordinary property of pozzolanic materials in consolidating marine  
86 structures (18).

87 Natural pozzolans were also a main component of *opus caementicium*, regarded as the  
88 precursor of modern concrete (7,10,19–24). The *opus caementicium* was used both to fill  
89 the void between outer brick or stone wall edges and for hydraulic structures (7,19,21,25–  
90 27). During the Imperial Age, it became the construction material for most of public works  
91 (28–32).

92 Starting from E. B. van Deman (33) pioneering work published in 1917, ancient Roman  
93 mortars have been attracting increasing interest from the scientific community. Despite this,  
94 the complex physical and chemical transformations involved in mortars hardening have not  
95 yet been fully understood. Significant progress, based on microscopic analysis, has been  
96 recently made (34–40). Specifically, the study demonstrates that the monuments built in  
97 Rome throughout the first four centuries AD (29) contain *Pozzolane Rosse*, scoriae erupted  
98 by the Alban Hills volcano during the mid-Pleistocene pyroclastic flow (30). Studies carried  
99 out on mortars manufactured using the same materials as in Trajan Markets in Rome have  
100 shown (34) a crystalline phase, strätlingite, growing at interfacial regions as a consequence  
101 of the pozzolanic reaction, thus providing significant mechanical improvement (34). The  
102 capability of strätlingite of distributing at interfaces positively influences the mechanical  
103 properties of mortar, contributing to block the propagation of cracks and microfractures  
104 (34,41). The observed behavior opens up new perspectives not only for a deeper  
105 understanding of the relationship between structure and properties in ancient Roman  
106 mortars, but also for designing new materials solutions for restoration and formulation of  
107 novel Portland-free sustainable mortars with superior performances in terms of durability  
108 and toughness.

## 109        **2.2. Nanolime in conservation of cultural heritage**

110    European cultural heritage (ECH) is of paramount importance. For this reason, ECH has to  
111    be protected following the main "Restoration Principles", outlined in international Charters  
112    (compatibility, recognition and little invasive). Materials deterioration can be prevented or  
113    slow down by conservative repairs, consisting in restoration and preventive treatments. So  
114    far, conservation science focused on polymer-based conservation materials. However,  
115    organic protectives are generally physically/chemically incompatible with the inorganic  
116    substrate. For this reason, nowadays, the application of inorganic nanomaterials such as  
117    calcium hydroxide nanoparticles in hydro-alcoholic dispersion (*nanolime*) are successfully  
118    introduced in CH for the consolidation of calcareous substrates, in order to reach a  
119    compromise between compatibility and efficacy of the intervention (42). Actually, nanolime  
120    presents the ability to penetrate deep into damaged zones, high reactivity and fast reactions  
121    in the carbonation process.

122    Procedure adopted to prepare nanolime particles mainly consists of chemical methods,  
123    carried out at high temperature and/or at high pressure, in aqueous, alcoholic or organic  
124    solvents (42–46). Recently, an innovative single-step process, based on an anion-exchange  
125    process, to produce nanolime in water at room temperature, has been patented (47). The  
126    nanolime, dispersed in ethanol, iso-propanol or water-alcohol mixtures, is composed by  
127    pure, crystalline and thin hexagonal lamellas (Fig.1). Recent studies reveal that the lamellas  
128    can be composed of nanoparticles <10nm in length and 6nm in thickness (48,49). Nanolime  
129    dispersions are successfully employed on wall paintings, stuccoes and frescoes and in the  
130    refurbishments of architectural surfaces (50–59). In particular, both in wall paintings and  
131    in frescoes, the nanolime guarantees a re-adhesion of detached paint layers on the wall  
132    substrate (42,50,51). Promising results are also obtained on stones and mortars, in terms  
133    of superficial consolidation as well as of reduction of water absorbed for capillarity (up to

134 70%), (53–59). Nanolime is able to penetrate up to some millimeters from the stone surface,  
135 filling the pores without occluding them. Moreover, when applied in diluted dispersions  
136 (<5g/l), nanolime does not produce relevant chromatic alteration on the stone surface.

137 From the results obtained in the different cases, the nanolime can represent a promising  
138 material for the restoration and preservation of the historic works of art, perfectly combining  
139 its consolidation efficacy with physico-chemical compatibility with the original historic lime  
140 based material.

### 141 **3. Waste management and recycling**

#### 142 **3.1 Recycled glass**

143 According to the United Nations glass waste represents about 7% of the total solid waste  
144 available; moreover, glass wastes occupy extensive parts of the landfills due to its non-  
145 biodegradable nature (60,61). In addition, the glass industry uses high amount of natural  
146 resources and energy and it produces high CO<sub>2</sub> emissions. Theoretically, glass can be  
147 recycled many times. Anyway, mixing different colored glass waste makes the recycling  
148 process unfeasible and highly expensive. Thus, concrete industry can represent a possible  
149 solution for an environmentally friendly management of glass wastes. Furthermore, the use  
150 of glass waste in construction appears among the most sustainable options since its use  
151 could reduce the environmental costs of concrete production.

152 Firstly, according to the chemical composition, glass waste should be suitable as raw  
153 material for cement production (62). Moreover, being amorphous (63) and with large  
154 quantities of silicon and calcium, glass is, in theory, pozzolanic if finely ground (63–68).  
155 Many studies (69–72) have confirmed that ground glass powder exhibits a good pozzolanic  
156 reactivity (69,70). Instead, the increase of finely ground glass content reduces strength of  
157 concrete at early ages due to slower pozzolanic reaction compared to cement hydration and

158 to a lower cement content (72,73); thus, different studies have investigated the optimum  
159 percentage of glass powder (5-30%) to replace cement, as well as the optimum particle size  
160 (0.1-100  $\mu\text{m}$ ). Based on the study of Shao (69,70), concrete with glass particles passing at  
161 38  $\mu\text{m}$  sieve replacing 30% of cement, exhibited higher strength than that with fly ash. Effects  
162 of glass color on strength are not evident; mechanical properties, in fact, are more related  
163 to physical characteristics than to slight difference in chemical compositions (74). Glass  
164 powder can contribute, after a proper curing, to a beneficial refinement of the pores (63,73)  
165 and a delay the penetration of ionic species (75–77). The only concern for using glass  
166 powder in cementitious materials is the potential alkali-silica reaction (*ASR*). Anyway,  
167 expansion tests carried out in most studies (69–76) showed that the *ASR* expansion  
168 decreased along with the percentage of glass powder due to its pozzolanic behaviour.

169 Glass waste (78) is an interesting to replace natural aggregates in concrete. Due to low  
170 absorption capacity, recycled glass aggregate is able to improve freeze–thaw resistance,  
171 drying shrinkage and abrasion (79). Idir *et al.* (79–84) found that a particle size less than 0.9-  
172 1 mm did not induce any harmful effect of *ASR* with a 20% of partial replacement of glass  
173 aggregate; with a lower particle sizes a higher percentage could be used safely (73). To  
174 avoid *ASR* reaction in concrete with glass aggregates, is necessary to reduce size of glass  
175 particles, glass content and using porous lightweight aggregate (84–89) or supplementary  
176 cementitious materials, including finely ground glass (80).

177 Several authors (71,90) studied the combined use of waste glass as a partial replacement  
178 of cement and aggregate in the same mixture. Shayan *et al.* (71) demonstrated that after  
179 increasing the glass powder (up to 30%) no effects of *ASR* were evident in a mixture with  
180 50% replacement of natural aggregate with waste glass. Recently, processes for the  
181 production of expanded glass particles have been developed and use of this lightweight  
182 aggregate for concrete has been proposed by several authors (85–89). Bertolini *et al.* (85)

183 demonstrated that the combination of expanded glass and silica fume led to a structural  
184 lightweight concrete showed a high resistance to the penetration of aggressive agents.  
185 Based on the results obtained in the reference (91), the same authors in a recent study (86)  
186 have verified also the possibility to manufacture lightweight mortars with expanded glass  
187 aggregates and glass powder in replacement of 30% cement. Preliminary results confirmed  
188 the beneficial effects of glass waste in terms of decreasing *ASR* expansion with respect to  
189 standard mortars (Figure 2).

### 190 **3.2 Aggregates from automotive shredder residues**

191 Every year in the world more than 50 Mt of End-of-Life Vehicles (ELV) are produced (92),  
192 as a consequence about 9 Mt of wastes are yielded. According to the European Directive  
193 (2000/53/EC) more than 95% (by mass) of ELV produced after 1979 shall be reused and  
194 recovered and more than 85% must be recycled. Nowadays, about 80-95% of ELV are  
195 subjected to a disassembling of glasses, transmission components, tires, seats and liquids  
196 drainage. At the shredding plant, an heterogeneous mix -"Automotive Shredder Residue"  
197 (ASHR)- is produced (93) constituted up to 75% of fine combustible materials with a calorific  
198 value higher than  $> 13$  MJ/kg (94). However, this waste is highly contaminated by heavy  
199 metals (**Errore. L'origine riferimento non è stata trovata.**) and often it contains mineral  
200 oils and fluids (95–100). In Europe, ASHR is classified as hazardous waste (2000-532-EEC  
201 directive).

202 As far as the inorganic fraction, excellent results have been obtained transforming the finest  
203 particles of ASHR (<4mm) into aggregates after a chemical treatment with calcium  
204 sulfoaluminate or Portland cement (101–103). Alunno Rossetti (101,102) pointed out an  
205 efficient process for aggregates production from ASHR, consisted of a preliminary  
206 separation step, where a fraction containing mainly inert and nonmetallic materials was  
207 sieved to obtain the required grading, followed by the mixing of this fraction with binding



208 materials and a superplasticizer agent, to produce granules of up to 2000 kg m<sup>-3</sup> of specific  
209 weight. These aggregates were employed to manufacture concrete with a 28-day  
210 compressive strength in the range 25-32 MPa (101,102,104) and noticeable freeze-thaw  
211 resistance (104).

### 212 **3.3 Recycled aggregates in concrete**

213 Concrete is one of the most widely used construction material in the world. In most cases,  
214 concrete elements are demolished at the end of their life, generating construction and  
215 demolition waste (CDW). Pure concrete waste can be obtained if all non-mineral dry building  
216 materials (plasterboards, wood, metals, plastics, glass) are removed before the demolition.  
217 All these extra materials can be recycled to produce eco-friendly plaster and mortars such  
218 as wood chips (105), waste glass (106,107), waste plastic particles (108,109), bricks (110).

219 Concerning structural concrete, several papers showed the suitability of reusing up to 30%  
220 coarse recycled aggregate particles for concrete strength classes up to 40 MPa (111–116).  
221 Moreover, a correlation between elastic modulus and compressive strength of recycled-  
222 aggregate concrete (RAC) was found in (112), showing that 15% lower elastic modulus is  
223 achieved by using 30% recycled aggregates, while tensile strength is reduced by 10% if the  
224 same concrete strength class is achieved by replacing 30% virgin aggregates with recycled  
225 concrete particles (111–115).

226 In terms of drying shrinkage, lower strains are detected especially for earlier curing times  
227 (111,112,117). Concerning time-dependent characteristics, creep behavior is more  
228 influenced by the presence of recycled aggregates than shrinkage, (114,118).

229 Even if 100% replacement of virgin aggregate is carried out by using particles coming from  
230 treatment of CDW, structural concrete can be prepared due to the positive effect on  
231 compressive strength achieved by adding fly ash/silica fume and an acrylic-based  
232 superplasticizer (111). Moreover, if fly ash is added to RAC, the volume of macro pores is

233 reduced, causing benefits in terms of mechanical performances such as compressive,  
234 tensile and bond strengths (111,115). In addition, fly ash proved to be very effective in  
235 reducing carbonation and chloride ion penetration depths in concrete, even in RAC (111).

236 Finally, on the basis of the results obtained through cyclic loading tests of beam–column  
237 joints, those made of RAC showed adequate structural behaviour (119,120). The previous  
238 encouraging results were obtained by using only coarse recycled aggregate, while, many  
239 authors found that in RAC the fine fraction is particularly detrimental to both mechanical  
240 performances and durability of concrete. For these reasons the more recent approach is to  
241 recycle for concrete production only the coarse recycled fraction. In several works (110,121–  
242 126) the possibility of reusing the fine fraction waste as aggregate for bedding mortars was  
243 evaluated (122,123). Mortars containing recycled fine aggregates develop lower mechanical  
244 strength with respect to the reference mixture, particularly when recycled bricks are used.  
245 Nevertheless, the bond strength (123–126) at the interface between the mortar and the brick  
246 comes out to be higher for mortars prepared with recycled aggregates.

247 A further opportunity can be the reuse of the very fine fraction (Figure 3) coming from  
248 recycling of CDW as filler for concrete, especially self-compacting mixtures (127–129). In  
249 particular, the rubble powder proved to be more promising with respect to limestone powder  
250 and fly ash as mineral addition for SCC. In conclusion, an optimization of the self-compacting  
251 concrete mixture seems to be achievable by the simultaneous use of rubble powder and  
252 coarse recycled aggregate.

### 253 **3.4 Artificial aggregates in concrete**

254 Industrial solid wastes (ISW) represent a widespread threat around the world due to the  
255 pollution to human health and the environment. The specific treatment of ISW plays an  
256 important role to maximize the efficiency of recycling processes (130,131). Among the  
257 different techniques, cold bonding pelletization is often proposed in low cost building

258 materials production (92). Particularly, one of the most interesting solution for waste  
259 recovery is the manufacture of recycled artificial aggregates (132–138). Cement-based cold  
260 bonding pelletization process has recently gained a relevant attention (102–104,139–142).  
261 The stabilization/solidification process uses a rotary plate pelletization pilot-scale apparatus  
262 with binding mixes. A double-step pelletization is performed in order to obtain final products  
263 with improved properties (143). Such process has been employed incorporating the waste  
264 content in the binding matrix from a minimum of 50% (wt. %) up to a maximum 70%.  
265 After this step, a second one is carried out with pure binder to encapsulate the aggregates  
266 (Figure 4) coming from the one step within an outer shell. This further step has proved to be  
267 very effective to improve the technological and leaching properties.  
268 Such approach has economic and environmental advantages due to the reduced energy  
269 requirement (process carried out at room temperature) respect to the industrial alternatives  
270 such as sintering (144,145), which is an energy intensive process. More recently, alternative  
271 cement-free binding matrices with reduced embedded CO<sub>2</sub> have been proposed for  
272 stabilization/solidification (146,147) such as geopolymer and alkali activated ones. These  
273 systems have gained an increasing interest from researchers thanks to promising results in  
274 terms of mechanical, physical, durability properties and possibility of synthesis starting from  
275 natural/industrial wastes (125,148) for a wide range of applications (149–153). A further  
276 reason of interest in cold bonding pelletization is a significant reduction of quarrying activities  
277 (154–159).  
278 Colangelo et al. (160,161) used municipal solid waste incinerator (MSWI) fly ash as raw  
279 materials while cement, lime and coal fly ash binders. According to Shi (160,161), a pre-  
280 washing treatment has been carried out to reduce the content of chlorides and sulfates  
281 contained in MSWI fly ash since the cementitious matrix has a reduced capability to  
282 immobilize chlorides and other soluble salts. The examined MSWI fly ash have been  
283 submitted to a two-step washing pre-treatment with liquid/solid ratio equal to 2:1 (160) in

284 order to reduce soluble salts content and the production of liquid waste. The MSWI fly ash  
285 samples, after washing pre-treatments, have been introduced in a pilot scale granulator  
286 apparatus having a rotating and tilting plate with a diameter of 80 cm in order to obtain the  
287 granules. The granules have been cured in a climatic chamber for 12 hours at 50°C and a  
288 relative humidity of 95%. Such phase gives the granules the necessary hardening to be  
289 used for the handling phase so it is very effective. Then, the granules have been cured for  
290 14 days at room temperature and humidity. Produced aggregates satisfied all the tests to  
291 be used in concrete industry.

### 292 **3.5 Recycled tires in concrete production**

293 The increasing number of vehicles on the roads generates about 1.4 billion of end-of-life  
294 tires (ELT) worldwide every year. The inadequate disposal of tires may be in some cases a  
295 potential threat to human health (fire risk, haven for rodents or other pests) and cause of  
296 environmental risks. The limited space and their potential for reuse has led many countries  
297 to impose a ban on the practice of landfilling. The estimated EU annual cost for the  
298 management of ELTs is € 600 million (162,163).

299 The tire is a complex and high-tech product representing a century of innovation, which is  
300 still on-going. Tire is made up of: (i) elastomeric compound, (ii) fabric and (iii) steel. The  
301 fabric and steel form the structural skeleton of the tire with the elastomer forming the “flesh”  
302 of the tire in the tread, side wall, apexes, liner and shoulder wedge. The elastomer is  
303 vulcanized and combined to chemicals and reinforcing fillers (e.g., carbon black) to further  
304 increase hardness (164).

305 Tyre rubber is resistant to mould, heat humidity, bacterial development, resistance to  
306 ultraviolet rays, some oils, many chemicals. Other features are the non-biodegradability,  
307 non-toxicity, elasticity. However, many of the characteristics, which are beneficial during on-

308 road life, are disadvantageous in post-consumer life and boost the transformation of this  
309 material from an environmental problem to engineering resource.

310 The recovery includes different options: i) “energy recovery” where ELTs, having a calorific  
311 value equivalent to that of good quality coal, are used as an alternative to fossil fuels, ii)  
312 “chemical processing” such as pyrolysis, thermolysis and gasification, and iii) “mass  
313 recovery”. The latter, when not applied in the form of whole tyres (such as for crash barriers)  
314 consists in a “granulate recovery” which involves tyre shredding and chipping, by which tyres  
315 are cut into small pieces of different sizes (shreds: 460-25 mm; chips: 76-13 mm; crumb  
316 rubber: 5-0.1 mm) (162). After the removal of the steel and fabric, the *recycled tyre rubber*  
317 (RTR) can be used for a variety of civil engineering projects such as, i.e., soft flooring for  
318 playgrounds and sports stadiums, modifiers in asphalt paving mixtures or additive/aggregate  
319 to Portland cement concrete. Among these, the addition (as crumb rubber) to asphalt  
320 mixtures is highly diffused due to the good chemical interaction, even leading to a partial  
321 dissolution (165). The recovery of RTR as aggregate in cement concrete has been  
322 discouraged so far by the not favorable interactions with the matrix and the loss of  
323 compression strength. However, these composites present many advantages and many  
324 reasons to address future research, as below discussed.

325 RTR used in cement concrete ranges from crumb rubber powders to rubber chips and is  
326 added to the cement paste by partial (or eventually total) replacement of the coarse or fine  
327 aggregates (165). The cement paste is mainly characterized by hydrated metal /semimetal  
328 oxides, thing that explains the hydrophilic nature (high surface energy). Rubber, instead,  
329 made of organic polymers, is characterized by a low surface energy, and therefore a  
330 hydrophobic character. The interaction hydrophilic-hydrophobic is very unfavorable resulting  
331 in a poor adhesion between rubber particles and the cement matrix. Figure 5 (top) shows  
332 SEM images of a typical sand based cement mortar and of a RTR added mortar (bottom):  
333 while a perfect adhesion can be appreciated between sand grains and cement paste, a

334 significant separation exists between the paste and the rubbery sites (166). For this reason,  
335 various rubber chemical treatments have been lately tested with the purpose of improving  
336 adhesion. Among these, treatments with NaOH (167–169), HNO<sub>3</sub> and cellulosic derivatives  
337 (170), or silane coupling agents (171) have been reported.

338 The significant loss of strength (reduction of 45 % upon 15 % of RTR addition (172,173) is  
339 mainly due to the fact that rubber sites are significantly softer than their surrounding media  
340 acting like “holes” inside the concrete. This critical property has limited so far the RTR  
341 added cement concrete to non-structural applications such as exterior wall materials,  
342 pedestrian blocks, lightweight aggregate in flowable fill for cement concrete, highway sound  
343 walls, residential drive ways, and garage floors (165).

344 An enhancement of toughness and ability to absorb impact energy has been observed with  
345 respect to conventional cement concrete (somewhere also explained and modeled), also in  
346 addition to an increased flexural strength (165,173).

347 The lightweight character of the rubberized concrete (due to the low specific weight of  
348 rubber), should be considered an advantage for the use as construction material since  
349 nowadays the structural efficiency is more important than the absolute strength level.  
350 Specifically, a decreased density for the same strength reduce the dead load, foundation  
351 size, and construction costs. Further, the low density enhances sound and thermal  
352 insulation, further properties relevant to construction applications (174).

353 The hydrophobic character of the rubber particles, although responsible of a difficult  
354 adhesion with the cement paste, has been recently proved (Figure 6) to strongly inhibit the  
355 absorption of water in rubberized mortars, which is instead instantaneous in the normal (i.e.  
356 sand containing) ones (166). This fact, which means higher freeze and thaw resistance,  
357 represents a further important key for future developments.

### 358 **3.6 Recycled polymers in cementitious mixtures**

359 Plastic products are used in almost every field, particularly in packaging, building and  
360 construction, automotive and electronics. However, the massive use of polymer products  
361 involves several environmental issues related to the plastic waste management and the  
362 possibility to reuse them. In the last decades, several studies investigated the use of plastic  
363 wastes in construction field. The use of recycled polymers in cementitious mixtures can be  
364 summarised in three different applications: I) polymeric fibers, II) plastic aggregates and III)  
365 polymer modified concrete.

366 The use of polymeric fibers in cementitious materials is able to overcome their brittle nature  
367 and cracking resistance. The properties of fiber reinforced cementitious composites (FRCC)  
368 depend on several fiber parameters such as: fibers amount (volume fraction), geometry  
369 (aspect ratio, surface texture etc.) and mechanical properties (depending on their nature).  
370 Moreover, also fibers durability in the alkaline environment and fiber/matrix bond play an  
371 important role in the fiber reinforced composite behavior. A great number of studies focused  
372 the attention on the use of fibers deriving from recycled PET, PVC, nylon and polyolefin  
373 (175–185). PET fibers present some durability issues in the alkaline environment (176,181)  
374 while the other common polymeric fibers (PP, PE, PVC etc.) are not chemically degraded in  
375 such environment. Considering compressive strength of FRCC, some authors reported a  
376 slight increase (177,183) while in other cases a decrease (178,180) of this property respect  
377 to unreinforced cementitious composites. The different results are explained by considering  
378 the ability of fibers to exert a confinement action, in the former cases, or the weak bond  
379 between fibers and the cementitious matrix, in the latter cases. On the contrary, splitting  
380 tensile strength and flexural strength of FRCC increase at increasing fibers volume fraction  
381 (177,178,180,186). Fresh properties of FRCC are greatly affected by fibers addition,  
382 depending on fibers volume fraction and geometry. Generally, fibers quantity increase  
383 determines a decrease of workability (178,183,186). Several studies focused the attention

384 on the investigation of the interfacial transition zone (ITZ) between fibers and cementitious  
385 matrix because synthetic fibers, have, in general, no chemical interactions with the  
386 cementitious matrix. Moreover, due to the smooth surface of traditional polymeric fibers, a  
387 very poor adhesion exists between the reinforcing phase and the matrix. To improve the  
388 adhesion and/or the interactions between fibers and the cementitious matrix two main  
389 approaches have been investigated: fibers mechanical deformation or surface chemical  
390 treatments but also ITZ densification. In the first case the aim is to increase surface contact  
391 area using crimped, twisted, fibrillated or embossed fibers (179,180). Fibers mechanical  
392 deformation increases friction during pull-out, delaying fiber/matrix debonding under load.  
393 ITZ densification provides a more uniform and continuous interphase between the two  
394 components while fibers chemical treatments, like graft copolymerization of acrylic acid,  
395 alkaline hydrolysis, nano-silica deposition and oxygen plasma, allow chemical interactions  
396 between fiber surface and cement paste (187–189). Finally, many authors investigated the  
397 use of recycled polymeric fibers to contrast shrinkage cracking phenomena in cementitious  
398 materials. Cracks number and area decrease at increasing fibers volume fraction depending  
399 also on fibers geometry and morphology (179,180,182).

400 Another viable strategy for polymeric wastes recycling is their use as aggregates in mortars  
401 or concrete. For this purpose, aggregates of different size (coarse and fine), geometry  
402 (pellets, flakes etc.) and polymeric nature (PET, PP, PS, HDPE, PVC etc.) have been  
403 investigated (155,174,190–199). On one side, using plastic aggregates is possible to obtain  
404 lightweight materials with a lower thermal conductivity, compared to traditional cementitious  
405 materials (174,190–192,196,198,200). Moreover, several authors reported also an  
406 improvement of acoustic isolation and impact resistance (175,190,191). Besides, plastic  
407 aggregates addition leads to a compressive strength decrease (155,174,190–198).  
408 However, also in this case, aggregates/matrix affinity plays a fundamental role and different



409 strategies have been proposed in the literature: the improvement of aggregates surface  
410 roughness, the densification of the ITZ or using expanded aggregates  
411 (155,174,191,193,194). In this particular case, aggregates open porosity is able to offer  
412 interlocking positions for the cementitious paste thus enhancing the adhesion and the  
413 homogeneity of the ITZ (155,174). However, several studies report about workability  
414 reduction of such composites resulting in poor compaction and thus porosity increase  
415 (155,191). Durability problems are strictly related to composites porosity and for this reason  
416 several authors describe an increase of water absorption, a decrease of freeze/thaw  
417 resistance and permeability to detrimental substances (CO<sub>2</sub>, chlorides ions, salts etc.)  
418 (191,194,196). However, some authors obtained good results in terms of abrasion and  
419 shrinkage resistance (191,195,197). Finally, attention must be paid also to compaction and  
420 segregation of plastic aggregates due to their low specific weight (199). As reported in  
421 literature, a viable strategy to avoid these phenomena is the use of fly ashes or silica fume  
422 but also using some additives (201–204) (superplasticizers, air entraining agent etc.).

423 In addition to polymeric fibers and aggregates, recycled polymers are also used as binder  
424 to produce the so called polymer modified concrete (PMC). The combination of conventional  
425 concrete and polymeric resins is able to overcome traditional drawbacks of cementitious  
426 materials like durability related issues, weak adhesion to substrates and low tensile strength  
427 (205,206). Several authors investigated the possibility to recycle PET by a glycolysis  
428 process to produce an unsaturated polyester resin to be used as binder in concrete or mortar  
429 preparation (207–209). Some interesting and promising results were obtained, such as a  
430 sharp decrease of water absorption at increasing PET content but also an increase of  
431 compressive strength at increasing resin content (208). Good effects were also reported in  
432 terms of porosity reduction, correlating such results to the porosity open to water and

433 porosity by N<sub>2</sub> absorption (209). More recently, a cement-less polymer concrete was  
434 investigated, using only recycled PP and recycled HDPE as binders (210).

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**TABLES**

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*Table 1 - ASHR composition*

Component	% (wt)	Element	% (wt)
PP	25	C	
PE	5	H	
PVC	10	Cl	
ABS	8	N	
PU	8	S	
PA	6	Heavy metals (ppm)	
Rubbers	9	Cd	69
Cables/wires	2	Cr	826
Metals	2	Cu	4800
Glass	24	Pb	2740
Other	1	Zn	6900

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