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## The Calcium looping process for low CO<sub>2</sub> emission cement plants

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### Abstract

The aim of this work is investigating the application of the Calcium looping process in cement plants with CO<sub>2</sub> capture. A novel configuration with oxyfuel calciner and a carbonator integrated in the raw meal suspension preheater has been assessed by means of process simulations. The results obtained show a high potential of the proposed process, with equivalent avoided CO<sub>2</sub> emissions (i.e. accounting for credits associated to electric power export) of about 94%, vs. 76% obtained for a competitive oxyfuel cement plant.

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### 1. Introduction

Cement production is the largest industrial source of carbon dioxide emissions, responsible for about 7% of the total CO<sub>2</sub> emission from large stationary sources. In cement plants, about 60% of the total CO<sub>2</sub> emissions arise from the calcination of the CaCO<sub>3</sub> in the raw meal feed (the remaining portion resulting from fuel combustion). Therefore, carbon capture and storage is the only option to significantly reduce the emission from cement plants.

Calcium looping is one of the most promising technologies for CO<sub>2</sub> capture in future short-medium term plants featuring the combustion of fossil fuels. Ca-looping is a regenerative process which takes advantage of the capacity of Calcium Oxide-based sorbents in capturing the CO<sub>2</sub> from combustion gases by means of sequential carbonation-calcination cycles. The process is carried out in two interconnected reactors operating at nearly atmospheric pressure. In the first one (the carbonator), CO<sub>2</sub> is removed from

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the gaseous phase at high temperatures (600-750°C) by Calcium Oxide, forming solid Calcium Carbonate according to the exothermic carbonation reaction ( $\text{CaO} + \text{CO}_2 \rightarrow \text{CaCO}_3$ ). In the second reactor (the calciner), the sorbent is regenerated according to the reverse endothermic reaction, sustained by oxycombustion of a carbon containing fuel. Thus, a highly concentrated  $\text{CO}_2$  stream is released from the calciner, ready for sequestration after proper purification.

A first option for cement plant emission reduction by Ca-looping process is to use the CaO-rich purge stream extracted from a power plant utilizing the Ca-looping process as a feed stream of the cement plant [1]. In this way,  $\text{CO}_2$  emission can be strongly reduced (well above 50%) with very limited modifications to the cement plant, because of both the avoided calcination of the feed (which is largely already calcined) and the reduced fuel input required. On the other hand, a large power plant needs to be present relatively close to the cement plant to transport this large amount of solids from the power to the cement plant. A second option is integrating the Ca-looping process in a stand-alone cement plant. This can be done by treating the flue gas in a carbonator placed either at the “end of pipe”, as already proposed in some works in the literature and object of a demonstration plant in Taiwan [2], or integrated within the raw meal suspension preheater. According to this second layout, the risers of the preheater are modified to work partly as carbonator reactors by including heat transfer surfaces and handle modified solid and gas flow rates. Such a configuration is object of a recent patent application from the authors [3-4].

The aim of this study is to present the first results of the integration of the Ca-looping process in a stand-alone cement plant, in a configuration where the process reactors are integrated in the raw meal preheating section. Energy efficiency and  $\text{CO}_2$  emissions are discussed and compared with those obtained for a plant with oxyfuel combustion, which represents the reference technology generally considered for  $\text{CO}_2$  capture in cement plants.

## 2. Plant description

The configuration of the innovative cement plant with  $\text{CO}_2$  capture by CaL process is shown in Fig. 1. Clinker is produced in a rotary kiln typical of state-of-the-art-plants, where the pre-calcined raw material is heated up to 1400-1450°C to initiate the reactions for clinker formation. Heat is provided by combustion of pet-coke at the hot end of the kiln. Hot combustion gases and solid species flows counter-currently in the kiln: solids move towards the hot end of the kiln thanks to its rotation around a slightly sloping axis, while gases flow in the opposite direction. The hot clinker exiting the kiln is cooled down in the clinker cooler by direct contact with ambient air. The combustion gases exit the kiln at around 1000-1050°C from the opposite side and cooled down by preheating the raw meal (i.e. the raw material for cement production, mainly constituted by  $\text{CaCO}_3$ ,  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{Fe}_2\text{O}_3$ ). Raw meal preheating is typically performed in a suspension preheater, where hot gas and cold solids are sequentially contacted in risers and separated in cyclones. While gas and solids flow co-currently in each riser, the preheating process is basically counter-current, since the solids entering at the top of the system descend through the preheater and are heated up, while the hot gas stream flows upwards and releases heat to the solids. In conventional cement plants, hot gases flowing through the preheater also include the gas from the pre-calciner, resulting from the combustion of part of the total fuel input (about 60% of the total) and from the  $\text{CO}_2$  of the decomposed limestone. In the proposed plant configuration, only the kiln flue gas is cooled in the suspension preheater, since limestone calcination is performed in a separate oxy-fired calciner.

The preheated raw meal exits the bottom stage of the suspension preheater and is sent to the oxyfuel pre-calciner, where limestone is decomposed to CaO and  $\text{CO}_2$ . About 55% of the resulting calcined raw meal is sent to the rotary kiln, while the remaining portion is re-injected in a proper position of the suspension preheater, where CaO can act as sorbent of the  $\text{CO}_2$  contained in the kiln flue gas. In this way, about 30% of this CaO is carbonated back to  $\text{CaCO}_3$  in this carbonation section (a high carbonation level was assumed considering the small particle size and the large flow of fresh limestone) before returning to

the pre-calciner, where it is released in the concentrated CO<sub>2</sub> stream. Therefore, the concentrated CO<sub>2</sub> stream released from the oxy-fired pre-calciner contains (i) the CO<sub>2</sub> from raw limestone calcination, (ii) the CO<sub>2</sub> from the oxyfuel combustion of the calciner fuel and (iii) the CO<sub>2</sub> initially contained in the kiln flue gases and captured in the carbonation section by the CaO sorbent. It must be highlighted that the carbonation section of the preheater line can require modifications of the conventional geometry to allow proper gas-solid contact times and include heat exchange surface for the absorption of the heat of the carbonation reaction. In particular, the carbonation section needs to be kept at a temperature of around 650°C to have proper reaction kinetics and chemical equilibrium leading to high CO<sub>2</sub> capture.

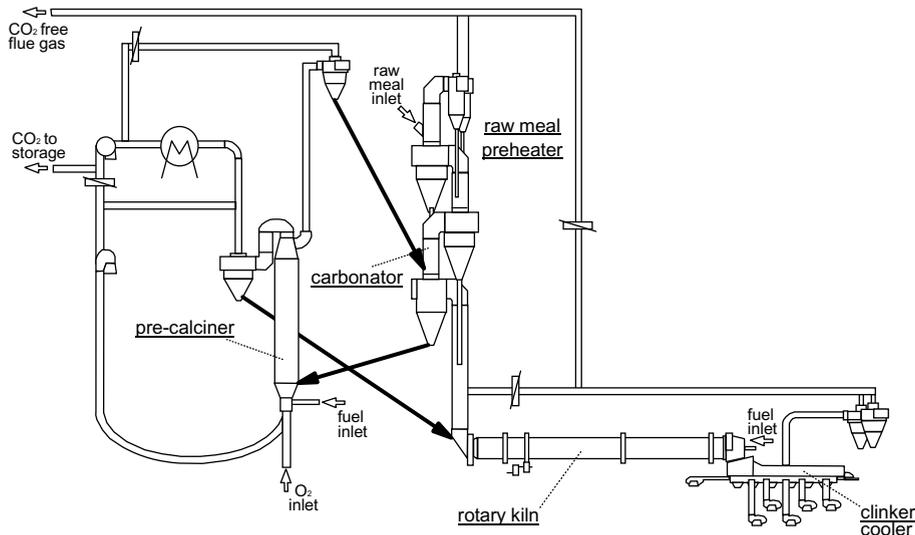


Fig. 1. Configuration of the innovative cement plant with CO<sub>2</sub> capture by Ca-looping process

### 3. Results

Mass and energy balances were calculated by means of the in-house process simulation code GS. The main results of the innovative plant proposed are resumed in Table 1 and compared with benchmark plants without CO<sub>2</sub> capture (first column) and with CO<sub>2</sub> capture by partial oxyfuel combustion (second column). The oxyfuel plant refers to a case similar to the CaL plant shown in Fig. 1, but no CaO is recycled to the suspension preheater to create a carbonation section in this case. Therefore, CO<sub>2</sub> generated in the kiln by fuel combustion and residual calcination is eventually emitted to the atmosphere. Such a configuration avoids some important drawbacks resulting from a full oxyfuel process (i.e. where also the combustion in the kiln is performed with a CO<sub>2</sub>/O<sub>2</sub>-based oxidant), which would suffer from high air in-leakages in the kiln, leading to low expected purities of the final CO<sub>2</sub>.

As shown in Table 1, the Ca-looping process allows capturing over 95% of the CO<sub>2</sub> produced in the plant, vs. about 82% of the oxyfuel plant. From another point of view, the specific emissions from the stack are equal to 94.9 g per kg of clinker produced, corresponding to 88.9% less than the reference plant without CO<sub>2</sub> capture and 52% less than the oxyfuel case. Such a high CO<sub>2</sub> capture level is obtained with a higher heat input, about 71% higher than the reference plant without capture and 35% higher than the oxyfuel cement plant. This increased fuel input leads to a large availability of waste heat which can be recovered by raising steam and generating electric power. Considering at first approximation a conversion efficiency of 43% from the heat recovered at temperature higher than 350°C and 30% for the lower

temperature heat (between 100 and 350°C), a gross power output of 1.22 kJ<sub>e</sub> and 0.60 kJ<sub>e</sub> per kg of clinker has been estimated for the CaL and the oxyfuel plants respectively. On a net basis, i.e. also including the auxiliary consumption from oxygen production (assumed equal to 200 kWh/t<sub>O2</sub>) and CO<sub>2</sub> compression (112 kWh/t<sub>CO2</sub>), a net export of 0.27 kJ<sub>e</sub>/kg<sub>clik</sub> has been obtained for the CaL case, vs. a net import of 0.10 kJ<sub>e</sub>/kg<sub>clik</sub> for the oxyfuel case. Considering also the additional CO<sub>2</sub> emission associated to the electric power import for the oxyfuel case and the avoided emission for electricity export to the grid for the CaL case, it is possible to calculate the equivalent CO<sub>2</sub> emission associated to clinker production. Assuming an average emission of 530 g/kWh, typical of the Italian power generation mix, the equivalent CO<sub>2</sub> emissions reduce to 54.4 g/kg<sub>clik</sub> for the CaL cement plant and increase to 215 g/kg<sub>clik</sub> for the oxyfuel plant. On the whole, the CaL cement plant allows reducing CO<sub>2</sub> emission by 93.8% with respect to the plant without CO<sub>2</sub> capture and by 75% with respect to the oxyfuel cement plant.

Table 1. Main results of the mass and energy balance of the Calcium looping cement plant and the benchmark plants without CO<sub>2</sub> capture and with CO<sub>2</sub> capture by oxyfuel combustion.

	State of the art cement plant w/o CO <sub>2</sub> capture	Oxyfuel calciner cement plant	Calcium looping cement plant
Fuel input, kJ <sub>LHV</sub> /kg <sub>clik</sub>	3230	4097	5531
Gross electric output, kJ <sub>e</sub> /kg <sub>clik</sub>	-	0.60	1.22
Auxiliaries, kJ <sub>e</sub> /kg <sub>clik</sub>	-0.21	-0.71	-0.95
Net power output, kJ <sub>e</sub> /kg <sub>clik</sub>	-0.21	-0.10	0.27
CO <sub>2</sub> capture efficiency, %	-	81.9	95.4
CO <sub>2</sub> emitted, g/kg <sub>clik</sub>	854.6	199.2	94.9
CO <sub>2</sub> avoided, %	-	76.7	88.9
Equivalent CO <sub>2</sub> emission, g/kg <sub>clik</sub>	884.8	214.7	54.4
Equivalent CO <sub>2</sub> avoided, %	-	75.7	93.8

#### 4. Conclusions

A new plant configuration for the production of cement with CO<sub>2</sub> capture by Calcium looping process has been presented in this work. A distinctive feature of the process is the high integration level of the carbonator reactor in the suspension preheater of the cement plant. From the mass and energy balances, CO<sub>2</sub> avoided emission of 89% has been obtained, with a net power output of 0.27 kJ<sub>e</sub>/kg<sub>clik</sub>, estimated by simplified assumptions on the heat recovery steam cycle. If the CO<sub>2</sub> credits from electric power export are taken into account, the equivalent CO<sub>2</sub> emissions are reduced by 94% with respect to the reference plant without CO<sub>2</sub> capture vs. 76% obtained for a competitive oxyfuel cement plant. The application of the Ca-looping process in cement plants in a highly integrated configuration is hence extremely promising for future low emission cement plants and certainly deserves further investigations.

#### References

- [1] Romano MC, Spinelli M, Campanari S, Consonni S, Cinti G, Marchi M, Borgarello E. The Calcium looping process for low CO<sub>2</sub> emission cement and power. *Energy Procedia* 2013; 37:7091–7099.
- [2] Chang MH, Huang CM, Liu WH, Chen WC, Cheng JY, Chen W, Wen TW, Ouyang S, Shen CH, Hsu HW. Design and Experimental Investigation of the Calcium Looping Process for 3-kW<sub>th</sub> and 1.9-MW<sub>th</sub> Facilities. *Chemical and Engineering Technology* 2013; 39(9):1525–1532.
- [3] Marchi MI, Cinti G, Romano MC, Campanari S, Consonni S. Improved process for the production of cement clinker and related apparatus (in Italian). *Patent application MI2012 A00382*.
- [4] Marchi MI, Cinti G, Romano MC, Campanari S, Consonni S. Process and improved plant for the production of cement clinker (in Italian). *Patent application MI2012 A00383*.