## Supporting information

## Sample dimensions

Sample dimensions for strut-only configurations are reported in Table 1. In Figure 1A the  $S_{1a-1b}$  and  $S_{x30^{\circ}}$  structures are shown as example.  $D_e$  and  $D_i$  are the external and internal diameters of the cylindrical body respectively, **L** is its length; **d** is the diameter of the struts, **p** and **n** are the spacing and the number of struts along the cylinder and  $\alpha$  is the inclination of criss-crossing struts.

Strut-only configurations							
Name	De	Di	L	d	р	n	α
S <sub>1a</sub>	20	17	66.67	2	3.37	20	-
S <sub>2a</sub>	20	17	66.67	1.5	3.37	20	-
S <sub>3a</sub>	20	17	66.67	1.2	3.37	20	-
S <sub>1a1b</sub>	20	17	66.67	2	3.37	20	-
S <sub>2a1b</sub>	20	17	66.67	1.7	3.37	20	-
S <sub>3a1b</sub>	20	17	66.67	1.4	3.37	20	-
S <sub>2a2b</sub>	20	17	66.67	1.5	3.37	20	-
S <sub>3a2b</sub>	20	17	66.67	1.3	3.37	20	-
S <sub>3a3b</sub>	20	17	66.67	1.2	3.37	20	-
S <sub>45°</sub>	20	17	66.67	2	3.37	20	-
Sx30°	20	17	66.67	1.6	6.7	8	30
Sx45°	20	17	66.67	1.5	6.7	8	45
Sx60°	20	17	66.67	1.6	6.7	5	60

**Table 1**. Samples dimensions for struts-only configurations.

Samples dimensions for ridges-only configurations are reported in Table 2. In Figure 1B, the  $R_{e 30^{\circ}, 20^{\circ}}$  structure is shown as example. As for struts-only configuration,  $D_e$ ,  $D_i$  and L are the external, internal diameter and length of the cylindrical body;  $\beta$  is the helix angle,  $\theta$  is the spacing between helixes and  $r_h$  is the helix radius.

 Table 2. Samples dimensions for ridges-only configurations.

Ridge-only configurations						
Name	De	Di	L	β	θ	r <sub>h</sub>
R <sub>e 30°,20°</sub>	20	17	66.67	30	20	0.65
Re 30°,45°	20	17	66.67	30	45	0.65
R <sub>e 30°,90°</sub>	20	17	66.67	30	90	0.65
Re 45°,20°	20	17	66.67	45	20	0.75
<b>R</b> e 45°,45°	20	17	66.67	45	45	0.75
R <sub>e 45°,90°</sub>	20	17	66.67	45	90	0.75
Re 60°,20°	20	17	66.67	60	20	0.825
Re 60°,45°	20	17	66.67	60	45	0.825
R <sub>e 60°,90°</sub>	20	17	66.67	60	90	0.825
<b>R</b> i 45°,20°	20	17	66.67	45	20	0.75
<b>R</b> i 45°,45°	20	17	66.67	45	45	0.75

<b>R</b> i 45°,90°	20	17	66.67	45	90	0.75
R <sub>x 30°,90°</sub>	20	17	66.67	30	90	0.65
<b>R</b> x 45°,90°	20	17	66.67	45	90	0.75
R <sub>x 60°</sub> ,90°	20	17	66.67	60	90	0.825

Samples dimensions for combined configurations can be obtained by combining the corresponding strut- and ridge-only designs.



Figure 1. Samples dimensions for struts-only (A) and ridges-only (B) configurations.

## Convergence analysis

Convergence analyses have been performed separately on strut- and ridge-only configurations with linearelastic assumptions.

Starting from strut-only configurations, convergence analysis for three-point bending has been performed on the  $S_{1a}$  structure. Results are shown in Figure 2 A, in which the reaction force is plotted as a function of the number of elements. According to it, the approximate mesh size chosen is of 1 mm on the outer wall and of 0.5 mm on the inner side, where struts are present.

Concerning ridges-only configuration, the analysis has been carried out on the  $\mathbf{R}_{e\,45^\circ,90^\circ}$  configuration. Results are shown in Figure 2 B, in which the reaction moment is plotted as a function of the number of elements. The approximate mesh size chosen is of 1 mm on the wall where there are no ridges, and of 0.5 mm where they are present.



**Figure 2**. Convergence analysis results: reaction force as a function of the mesh size are reported for the  $S_{1a}$  structure (A) and for the Re 45°,90° configuration (B). The chosen mesh size is the one highlighted by the big solid dots.