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(54) **ABRASIVE WATER-JET CUTTING MACHINE AND METHOD, AND COMPOSITION COMPRISING ABRASIVE MATERIAL**

ABRASIVE WASSERSTRAHLSCHNEIDEMASCHINE UND -VERFAHREN, SOWIE ZUSAMMENSETZUNG MIT PULVERFÖRMIGEN ABRASIVEN PARTIKELN

MACHINE ET PROCÉDÉ DE DÉCOUPE À JET D'EAU ABRASIF, ET COMPOSITION COMPRENANT DES PARTICULES ABRASIVES

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Description

[0001] The present invention relates to an abrasive water-jet cutting machine according to the preamble of claim 1, such a machine being known from WO 2018/060920 A1, a composition according to the preamble of claim 11, also known from WO 2018/060920 A1, and an abrasive water-jet cutting method comprising the use of such a composition.

Background art

[0002] Abrasive water-jet cutting machines are machine tools which cut and shape workpieces by means of a jet of a water-abrasive material mixture. Such a technology is known as "Abrasive Water Jet" (AWJ).

[0003] Abrasive water-jet cutting machines generally comprise:

- pumping means, which can be fluidically connected to a water source, for the generation of a pressurized water flow;
- a cutting head, comprising a primary nozzle, a mixing chamber and a focusing nozzle, wherein the pressurized water flow originating from the pumping means is conveyed into the primary nozzle of the cutting head in which the pressure energy of the pressurized water flow is converted into kinetic energy so as to form a water jet, and wherein said water jet is then conveyed into the mixing chamber;
- a gravity dispensing system of powdered abrasive material, comprising
 - a tank (e.g. a hopper) containing powdered abrasive material,
 - a feeding pipe, fluidically connecting the tank to the mixing chamber of the cutting head,

wherein the abrasive powder material gravity dispensing system dispenses said abrasive powder material into the mixing chamber of the cutting head via the feeding pipe;

wherein the cutting head mixes, in the mixing chamber, the powdered abrasive material with the water jet forming a water-abrasive material mixture jet, and said cutting head dispenses the water-abrasive material mixture jet by means of the focusing nozzle.

[0004] The gravity dispensing systems of powdered abrasive material have several critical issues. In particular, such systems are excessively inconvenient when they are used to perform finer and more precise cutting operations, i.e. for so-called microabrasive water jet (μ AWJ) cutting operations.

[0005] Specifically, μ AWJ operations require the use of low-abrasive mass flow rates (less than 20 g/min) and the use of powdered abrasive material with a finer grain size (mesh greater than #200) as compared to the usual one for macro applications (which instead use meshes in the range from #80 to #120).

[0006] Gravity dispensing systems cannot guarantee a smooth and reliable supply of abrasive material for μ AWJ operations. Indeed, gravity dispensing systems have a variability in the dispensing of abrasive material mass flow rate which reaches values around 10%, which is not acceptable for μ AWJ operations.

[0007] Furthermore, abrasive water jet cutting machines are often actuated by means of actuating systems, such as beam, gantry, six-axis robotic arm, and such actuating systems, when characterized by fast dynamics, generate further critical issues in the constant supply of powdered abrasive material. Furthermore, gravity dispensing systems for powered abrasive material are incompatible with the use of the machine tool in "overhead" configuration (implemented, for example, by six-axis robots).

[0008] A further critical issue of these dispensing systems derives in that the powdered abrasive material dispensed by the dispensing system, which is particularly hygroscopic, is negatively exposed to the presence of environmental and process humidity present within the pipes into which the powdered abrasive material is conveyed.

[0009] In particular, at the interface between the feeding pipe and the mixing chamber of the cutting head, the hygroscopicity of the powered abrasive material causes the agglomeration of a stationary layer of powdered abrasive material on the inner wall of the feeding pipe, which progressively reduces the useful section for dispensing the abrasive material into the mixing chamber, whereby causing undesired changes in the abrasive material mass flow rate.

[0010] Furthermore, the layer of powdered abrasive material agglomerated on the inner wall of the feeding pipe is subject to the risk of sudden detachments, which contribute to produce undesirable variations in the abrasive material mass flow rate, and which, in the most serious cases, can cause clogging of the focusing nozzle of the cutting head and damage to the machine tool.

[0011] An attempt was made to overcome these problems through the use of abrasive material dispensing systems according to the "Abrasive Suspension Jet" (ASJ) technology, in which the abrasive powder material is previously dispersed in a dispersion liquid (e.g. water), so as to form a hydro-abrasive mixture stored in a tank. Such a hydro-abrasive mixture is then dispensed through a single nozzle to form a pressurized jet of hydro-abrasive mixture.

[0012] However, such an abrasive dispensing system can only be used at low pressures (less than 100 MPa), which

are not high enough to perform the precision cutting required in μ AWJ applications.

[0013] Furthermore, in order to ensure adequate dispersion of the powdered abrasive material in the dispersion substance, avoiding unwanted sedimentation, the mass ratio between the powdered abrasive material and the dispersion liquid of the aforesaid hydro-abrasive mixtures must be very low. This determines an exaggerated use of dispersion liquid in order to adequately disperse (and dispense) a low quantity of abrasive material in powder form.

[0014] It is the object of the present invention to provide an abrasive water-jet cutting machine, and in particular for μ AWJ machining, provided with an abrasive material dispensing system having such features as to solve at least some of the drawbacks of the prior art.

[0015] It is a particular object of the present invention to provide such a dispensing system of powdered abrasive material as to ensure a regular and reliable dispensing of powdered abrasive material, even at low dosages of powdered abrasive material (less than 20 g/min).

[0016] It is a further particular object of the present invention to provide a dispensing system of powdered abrasive material compatible with the use of the machine tool in "overhead" configuration.

[0017] It is a further particular object of the present invention to provide a dispensing system of powdered abrasive material in which stationary agglomerations of powdered abrasive material are avoided, and other critical issues deriving from the exposure of the powdered abrasive material to both environmental and process humidity present within the pipes into which the powdered abrasive material is conveyed.

[0018] It is a further particular object of the present invention to provide a dispensing system of abrasive material which can also be used at the pressures required to perform processes of the μ AWJ type (over 380 MPa).

[0019] It is a further particular object of the present invention to provide a dispensing system of powdered abrasive material which uses a smaller amount of dispersion substance to adequately dispense a larger amount of powdered abrasive material.

Detailed description of the invention

[0020] The present invention relates to an abrasive water-jet cutting machine provided with an abrasive material dispensing system according to claim 1. The dependent claims relate to advantageous and preferred embodiments.

[0021] A further disclosed aspect is a composition according to claim 11 which comprises a powdered abrasive material dispersed in a gelatinous fluid, as well as the use of said composition in an abrasive water-jet cutting method, as per claim 14.

[0022] According to an aspect of the invention, the abrasive water-jet cutting machine comprises:

- pumping means, which can be fluidically connected to a water source, for the generation of a pressurized water flow;
- a cutting head, comprising a primary nozzle, a mixing chamber and a focusing nozzle,
- wherein the pressurized water flow originating from the pumping means is conveyed into the primary nozzle of the cutting head in which the pressure energy of the pressurized water flow is converted into kinetic energy so as to form a water jet, and wherein said water jet is then conveyed into the mixing chamber;
- a dispensing system of powdered abrasive material, comprising:
 - a tank containing powdered abrasive material,
 - a feeding pipe, fluidically connecting the tank to the mixing chamber of the cutting head,
 - a dispenser, dispensing the powdered abrasive material contained within the tank into the mixing chamber by means of the feeding pipe;

wherein the cutting head mixes, in the mixing chamber, the abrasive material with the water jet forming a water-abrasive material mixture jet, and said cutting head dispenses the water-abrasive material mixture jet by means of the focusing nozzle.

wherein the powdered abrasive material contained in the tank is homogeneously dispersed in suspension in a gelatinous water-based fluid;

and wherein the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid is comprised between 1.0 and 3.5, or between 1.5 and 3.0, preferably between 2.0 and 2.5.

[0023] Such a configuration of the dispensing system, and in particular of the abrasive material dispensed thereby, allows the control of the hygroscopic properties of the abrasive material. Indeed, since the powdered abrasive material is homogeneously dispersed in the water-based gelatinous fluid, it is completely saturated with water, and therefore it is immune to the critical issues deriving from its exposure to environmental and process humidity.

[0024] Furthermore, since the powdered abrasive material is completely saturated with water and is homogeneously dispersed in the water-based gelatinous fluid, said dispensing system dispenses the abrasive material in a regular and

reliable manner, even at small doses of abrasive material (less than 20 g/min).

[0025] Furthermore, such a dispensing system is compatible with the use of the cutting machine in "overhead" configuration.

[0026] Furthermore, since the dosage of abrasive powder material evenly dispersed in the water-based gelatinous fluid has a mass ratio of between 1.0 and 3.5, said dispensing system uses a smaller amount of dispersion substance to adequately dispense a larger amount of powdered abrasive material.

[0027] Last but not least, such a dispensing system can also be used at the pressures required to perform μ AWJ operations (above 380 MPa).

[0028] In order to understand the invention and better appreciate its advantages, the description of some non-limiting embodiments will be provided below with reference to the figures, in which:

- figure 1 schematically shows the abrasive water-jet cutting machine, according to an embodiment of the invention;
- figure 2A is a front view of a cutting head according to an embodiment of the invention;
- figure 2B is an axial section view of the cutting head shown in figure 2A;
- figure 3A is a front view of an injector member according to an embodiment of the invention,
- figure 3B is an axial section view of the injector member shown in Figure 3A;
- figure 4 is a longitudinal section view of the assembly cutting head-injector member assembly;
- figure 5A is a front view of a dispensing system according to an embodiment of the invention;
- figure 5B is an axial section view of the dispensing system shown in figure 5A;
- figure 6 shows a sample of material cut by means of the abrasive water-jet cutting machine, according to an embodiment of the invention;
- figure 7 shows two samples of the same material, cut with an abrasive water-jet cutting machine according to the prior art and according to the invention.

[0029] With reference to the figures, an abrasive water-jet cutting machine according to the invention is indicated by reference numeral 1 as a whole.

[0030] According to an aspect of the invention, the abrasive water jet cutting machine 1 comprises pumping means 2, which can be fluidically connected to a water source 3, for the generation of a pressurized water flow 4.

[0031] The cutting machine 1 further comprises a cutting head 5, comprising a primary nozzle 27, a mixing chamber 6 and a focusing nozzle 7.

[0032] According to an aspect of the invention, the pressurized water flow 4 originating from the pumping means 2 is conveyed into the primary nozzle 27 of the cutting head 5 in which the pressure energy of the pressurized water flow 4 is converted into kinetic energy so as to form a water jet 12, and wherein said water jet 12 is then conveyed into the mixing chamber 6.

[0033] The cutting machine 1 further comprises a dispensing system 8 of powdered abrasive material, which comprises a tank 9 containing abrasive material, a feeding pipe 10, which fluidically connects the tank 9 to the mixing chamber 6 of the cutting head 5, a dispenser 11, which dispenses the powdered abrasive material contained within the tank 9 into the mixing chamber 6 by means of the feeding pipe 10.

[0034] According to a further aspect of the invention, the cutting head 5 mixes, in the mixing chamber 6, the abrasive material with the water jet 12 forming a water-abrasive material mixture jet 13, which is dispensed by the cutting head 5 by means of the focusing nozzle 7.

[0035] The focusing nozzle 7 also has the task, following the mixing of the abrasive material with the water jet 12, of increasing mixing efficiency and transferring of momentum from the water jet 12 to the abrasive material.

[0036] According to a further aspect of the invention, the powdered abrasive material contained in the tank 9 is homogeneously dispersed in suspension in a gelatinous water-based fluid 60.

[0037] According to a further aspect of the invention, the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid 60 is from 1.0 to 3.5.

[0038] Such a configuration of the dispensing system 8, and in particular of the abrasive material dispensed thereby, allows the control of the hygroscopic properties of the powdered abrasive material. Indeed, since the powdered abrasive material is homogeneously dispersed in the water-based gelatinous fluid 60, it is completely saturated with water, and therefore it is immune to the critical issues deriving from its exposure to environmental and process humidity.

[0039] Furthermore, since the powdered abrasive material is completely saturated with water and is homogeneously dispersed in the water-based gelatinous fluid 60, said dispensing system 8 dispenses the abrasive material in a regular and reliable manner, even at small doses of abrasive material (less than 20 g/min).

[0040] Furthermore, such a dispensing system 8 is compatible with the use of the cutting machine 1 in "overhead" configuration.

[0041] Furthermore, since the dosage of abrasive powder material evenly dispersed in the water-based gelatinous fluid 60 has a mass ratio of between 1.0 and 3.5, the dispensing system 8 uses a smaller amount of dispersion substance

with respect to the abrasive material dispensing systems according to ASJ technology, to adequately dispense a larger amount of powdered abrasive material.

[0042] Last but not least, such a dispensing system 8 can also be used at the pressures required to perform μ AWJ processes (above 380 MPa).

[0043] According to a further embodiment, the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid 60 in which the powdered abrasive material is uniformly dispersed is approximately 2.0.

[0044] According to an embodiment, the particle size of the powdered abrasive material homogeneously dispersed in suspension in the gelatinous water-based fluid 60 is less than #200 mesh, preferably is comprised between #350 mesh and #600 mesh.

[0045] The average size of granules of abrasive powder material is less than 70 micrometers, preferably between 15 and 60 micrometers.

[0046] The nature and chemical composition of the abrasive material used can be of different types, e.g. natural minerals, such as Almandine Garnet or Olivine, synthetic, ceramic, such as Silicon Carbide, metal compounds, biological material.

[0047] The water-based gelatinous fluid 60 consists of distilled water and a gelling agent (e.g. a polymer) in sufficient quantity to keep the mixture in suspension without the granules of powdered abrasive material settling on the bottom of tank 9.

[0048] According to an embodiment of the invention, the cutting head 5 comprises a substantially tubular mixing chamber 6, which forms a front surface 14, a rear surface 15 parallel to the front surface 14, and a peripheral surface 29.

[0049] The terms "front" and "rear" refer to the direction of the pressurized water flow 4 through the cutting head 5.

[0050] The mixing chamber 6 forms a front seat 16 at the front surface 14 and a rear seat 17 at the rear surface 15, wherein the front and rear seats 16, 17 are substantially cylindrical in shape.

[0051] Furthermore, the mixing chamber 6 forms a water inlet opening 18 at the front seat 16, and a mixture outlet opening 19 at the rear seat 17.

[0052] The mixing chamber 6 forms a jet channel 20, transverse to the front surface 14 and to the rear surface 15, and in flow communication with the front seat 16 and the rear seat 17 by means of the water inlet opening 18 and the mixture outlet opening 19.

[0053] The jet channel 20 and the front seat 16 form a front shoulder 21 at the water inlet opening 18. Furthermore, the jet channel 20 and the rear seat 17 form a rear shoulder 22 at the mixture inlet opening 19.

[0054] A primary nozzle housing 23 is accommodated inside the front housing 16, abutting against the front shoulder 21.

[0055] The primary nozzle housing 23 is substantially cylindrical in shape, and defines a front base 24 and a rear base 25, wherein the rear base 25 abuts against the front shoulder 21.

[0056] The primary nozzle housing 23 forms a primary nozzle seat 26 at the front base 24.

[0057] A primary nozzle 27 is accommodated in the primary nozzle housing 26. The primary nozzle 27 converts the pressurized water flow 4 from the pumping means 2 into the water jet 12.

[0058] The focusing nozzle 7 forms a focusing channel 28 to concentrate the water jet 12.

[0059] The focusing nozzle 7 is arranged in the rear seat 17 and locked by interference. Advantageously, such a locking interference ensures correct centering and positioning of the focusing nozzle 7 with respect to the primary nozzle 27.

[0060] The mixing chamber 6 forms an injection opening 30 at the peripheral surface 29, and the injection opening 30 is transverse to the jet channel 20 and connected fluidly to the jet channel 20.

[0061] The cutting head 5 further comprises a retaining flange 31, forming a cavity 32 which holds and seals inside the mixing chamber 6. Furthermore, the retaining flange 31 forms a second injection opening 33, which is configured concentrically with respect to the injection opening 30 of the mixing chamber 6.

[0062] The injection opening 30 and the second injection opening 33 allow the injection of the abrasive dispersed in the water-based gelatinous fluid 60 into the mixing chamber 6 by means of a connection with the feeding pipe 10.

[0063] According to an embodiment of the invention, the feeding pipe 10 is connected, at a first end 34 thereof, to the tank 9, and is connected, at a second end 35 thereof, to an injector member 36.

[0064] According to an embodiment of the invention, the injector member 36 comprises an injector housing 37 and an injector nozzle 38.

[0065] The injector housing 37 forms a connection portion 39 adapted to connect the injector member 36 to the feeding pipe 10.

[0066] In addition, the injector housing 37 forms a shaped channel 40 inside adapted to accommodate the injector nozzle 38.

[0067] The injector nozzle 38 forms an injection channel 41 therein, and an end portion 45 of the injector nozzle 38 is configured to protrude into the jet channel 20 of the mixing chamber 6, so that the injection channel 41 fluidically connects the feeding pipe 10 to the jet channel 20.

[0068] According to an embodiment of the invention, the end portion 45 of the injector nozzle 38 extends by a fraction

of millimeters, preferably 0.5 mm, within the jet channel 20. Advantageously, this allows the abrasive material, dispersed in the water-based gelatinous fluid 60, to be conveyed in the immediate vicinity of the water jet 12. Therefore, the conveyed abrasive does not accumulate on the walls of the jet channel 20 and is not released suddenly.

5 [0069] The positioning and connection of the injector nozzle 38 to the mixing chamber 6 is ensured by means of a threaded joint, bayonet connection or other connection system which guarantees robustness and complete sealing.

[0070] According to an embodiment of the invention, the shaped channel 40 comprises an end portion 42, which forms an air injection channel 43 concentric to the end portion 42, and a coupling portion 61 adapted to achieve a shape coupling with the injector nozzle 38.

10 [0071] Advantageously, the concentric configuration of the air injection channel 43 compared to the end portion 42 reduces the overall dimensions of the injector member 36.

[0072] Further advantageously, the concentric configuration of the air injection channel 43 allows an optimal projection of the abrasive material dispersed in the water-based gelatinous fluid 60 towards the water jet 12, whereby keeping the air injection channel 43 clean and functioning.

15 [0073] The air injection channel 43 forms a gap 44, between the air injection channel 43 and the end portion 45 of the injector nozzle 38.

[0074] Furthermore, the injector housing 37 forms an airflow channel 47 which flows into the air injection channel 43, and which forms a connection housing 46.

20 [0075] The air flow channel 47 is connected to a pneumatic conduit 48 at the connection seat 46. Advantageously, the inner diameter of the pneumatic conduit 48 is substantially identical to the diameter of the airflow duct 47, so as to avoid steps that could negatively impact on the airflow.

[0076] On the pneumatic conduit 48 there is a valve 49 which regulates the air flow entering the air flow duct 47. The air flow entering the air flow channel 47 is sucked in by the passage of the water jet 12 by Venturi effect.

[0077] Furthermore, the pneumatic conduit 48 is provided with a pressure gauge 50 and a flow meter 51 (either analog or digital) to monitor and allow the control of the air flow introduced into the pneumatic conduit 48.

25 [0078] Advantageously, by means of the control valve 49 it is possible to reduce the flow of air entering the pneumatic conduit 48, so as to reduce the air dosage of the water jet 12. In such a manner, the Venturi effect generated by the water jet 12 can propagate to the abrasive material dispersed in the water-based gelatinous fluid 60, which is therefore sucked into the mixing chamber 6 without the intervention of a possible upstream thrust.

30 [0079] Such a configuration of the pneumatic conduit 48 can also be used for checking the assembly of the cutting head 5, for monitoring the state of wear of the components (e.g. the injector nozzle 38, the primary nozzle 27, the mixing chamber 6 and the focusing nozzle 7) and for checking the correct execution of the cut in real time.

35 [0080] In order to check assembly, it is necessary to completely prevent the access of air into the mixing chamber 6, so as to measure the level of pressure generated inside the mixing chamber 6 by the passage of the water jet 12. Pressure values higher than, equal to or close to atmospheric value indicate an incorrect alignment of the components, with probable contact between the water jet 12 and the channel and the inner walls of the jet channel 20 or the focusing nozzle 7. Values closer to vacuum (e.g. 0.2 or 0.1 absolute bar) indicate a valid alignment of the components, which generate a significant Venturi effect.

40 [0081] In order to check the state of wear of the components, it is necessary to record the pressure changes in the mixing chamber 6 over an extended period to determine the drift of wear of the components of the cutting head 5. In particular, a less pronounced Venturi effect in the jet channel 20 reveals the progressive wear of the primary nozzle, with a consequent decrease in the outflow velocity of the water jet 12.

45 [0082] In order to check the correct execution of the cut in real time, it is necessary to record the punctual pressure variations in the mixing chamber. Such events can be traced back to malfunctions in the water jet dispensing system 12 of the abrasive material dispersed in the water-based gelatinous fluid 60 or of the air injected through the air flow channel 47. By evaluating these phenomena, it is possible to determine the correct function of the water jet 12 at any time, so as to predict the success of the cutting operation and, if not, interrupt the cut.

[0083] According to an embodiment of the invention, the tank 9 is a vessel with a substantially cylindrical shape.

50 [0084] According to a preferred embodiment, the tank 9 is configured in the form of a syringe, and comprises a cylindrical portion 52, within which the abrasive material dispersed in the water-based gelatinous fluid 60 is loaded and stored, and a cannula portion 53.

[0085] According to an embodiment, the nozzle 11 is configured as a plunger organ 54, which is slidingly arranged within the cylindrical portion 52, and is configured so as to push the abrasive material dispersed in the water-based gelatinous fluid 60 contained in the cylindrical portion 52 of the tank 9 towards the cannula portion 53.

55 [0086] The cannula portion 53 is connected to the first end 34 of the feeding pipe 10 in order to make a fluidic connection between the tank 9 and the feeding pipe 10.

[0087] According to a preferred embodiment, the plunger member 54 is configured to apply a thrust pressure of about 1 relative bar.

[0088] Advantageously, using such a pressure value causes the abrasive material dispersed in the water-based

gelatinous fluid 60 to be substantially incompressible, therefore the advancement rate of the plunger member is easily and directly correlated to the flow rate of abrasive material dispersed in the water-based gelatinous fluid 60.

[0089] According to an embodiment, the dispensing system 8 comprises an auxiliary filling syringe, adapted to recharge the tank 9 in real time, i.e. to fill the tank 9 with new abrasive material dispersed in the water-based gelatinous fluid 60 at the same time as the execution of a cutting process by the same cutting machine 1.

[0090] Preferably, such a real time filling is performed in a period of time between the machining of two successive geometries belonging to the same component under construction or to different components.

[0091] According to a further embodiment, the dispensing system 8 comprises an abrasive tank dedicated to the storage of abrasive material and a gel tank dedicated to the storage of water-based gelatinous fluid, in which the simultaneous mixing and pressurization of the abrasive material with the water-based gelatinous fluid takes place in the feeding pipe 10, through a "turbulent" path.

[0092] Advantageously, the tank 9 is filled at source by means of an auxiliary dispenser to avoid the presence of air bubbles or other gases.

[0093] Furthermore, a rear relief valve 56 is arranged on the plunger member 54 to evacuate possible air or other gas bubbles present in the gelatinous water-based fluid 60 inside which the abrasive material is dispersed, which may introduce compressibility or cause interruptions in the feeding of the abrasive material dispersed into the gelatinous water-based fluid 60 at the cutting head 5.

[0094] The plunger member 54 is connected to a motor 58, preferably electric, by means of a transmission 57.

[0095] According to a preferred embodiment, a flow stop valve 59 is connected to the feeding pipe 10. The flow stop valve 59 is designed to either stop or divert the flow of abrasive material dispersed in the water-based gelatinous fluid 60 in an emergency.

[0096] Advantageously, in such a manner it is possible to stop the injection of abrasive material dispersed in the water-based gelatinous fluid 60 into the cutting head 5, also if the dispensing system 8 continues to dispense abrasive material dispersed in the water-based gelatinous fluid 60 from tank 9.

[0097] With further advantage, the flow stop valve 59 has the auxiliary function of interrupting any upward flow from the cutting head 5, e.g. of air or water in the event of obstruction of the focusing nozzle 7, so as to protect the dispensing system 8 from overpressure damage.

[0098] According to a further aspect, the present invention relates to a composition comprising a powdered abrasive material homogeneously dispersed in suspension in a gelatinous water-based fluid 60, wherein the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid 60 is from 1.0 to 3.5, or approximately 2.0 and wherein the particle size of the powdered abrasive material dispersed in suspension in the gelatinous water-based fluid 60 is from #350 mesh to #600 mesh.

[0099] Preferably, the average size of granules of abrasive powder material in said composition is comprised between 15 and 60 micrometers.

[0100] A further object of the present invention relates to an abrasive water jet cutting method, wherein said method comprises the use of the abrasive composition according to the present invention.

[0101] Of course, a person skilled in the art can make further changes and variants all contained within the scope of protection defined by the claims in order to satisfy contingent, specific needs.

[0102] Hereinafter, some experimental tests carried out with the abrasive water jet cutting machine and the composition including the abrasive material disclosed herein will be described, aimed at highlighting effectiveness and technical advantages.

Example 1: Cutting test on 2.0-mm thick austenitic stainless steel (AISI 301 / EN 1.4310)

[0103] The cutting test is performed on 2.0-mm thick austenitic stainless steel (AISI 301 / EN 1.4310) to verify the performance of the disclosed cutting machine on relatively thick material.

[0104] Indeed, 2.0 mm is close to the maximum thickness which can be cut with μ AWJ cutting machines of the background art known to inventors.

[0105] The kerf geometry and the cut wall surface roughness are measured at different depth levels:

- at 0.2 mm from the top ("top")
- at mid-height (1.0 mm, "mid")
- at 0.2 mm from the bottom ("bot")

[0106] The test results are shown in tables 1.1 and 1.2 below.

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Table 1.1: Cutting tests on 2-mm thick austenitic stainless steel (AISI 301 / EN 1.4310) Macro-geometric verification of cutting wall as advancement rate varies.

Austenitic stainless steel (AISI 301 / EN 1.4310), 2.0 mm thick Kerf width inspection				
V_f [mm/min]	W_{top} [mm]	W_{bot} [mm]	$W_{average}$ [mm]	<i>Taper</i> [mm]
3	0.187	0.221	0.204	-0.015
6	0.172	0.158	0.165	0.007
9	0.171	0.145	0.158	0.013
12	0.165	0.128	0.146	0.018
15	0.164	0.116	0.140	0.024
18	0.157	0.108	0.133	0.024
21	0.153	0.093	0.123	0.030
24	0.152	0.090	0.121	0.031
V_f : head advancement rate W_{top} : upper kerf width W_{bot} : lower kerf width $W_{average}$: average kerf width <i>Taper</i> : single wall taper				

Table 1.2: Cutting tests on 2-mm thick austenitic stainless steel (AISI 301 / EN 1.4310) Roughness verification of cutting wall as advancement rate varies.

Austenitic stainless steel (AISI 301 / EN 1.4310), 2.0 mm thick Roughness inspection								
V_f [mm/min]	R_a top [μm]	R_a mid [μm]	R_a bot [μm]	R_a average [μm]	R_z top [μm]	R_z mid [μm]	R_z bot [μm]	R_z average [μm]
3	0.36	0.44	0.56	0.45	3.02	3.15	4.00	3.38
6	0.38	0.49	0.64	0.51	3.28	3.95	5.01	4.01
9	0.42	0.48	0.64	0.51	3.61	3.70	4.77	3.92
12	0.44	0.59	0.81	0.67	3.77	4.34	5.90	5.05
15	0.47	0.66	0.96	0.72	3.98	5.16	6.47	5.25
18	0.49	0.83	1.27	0.90	3.90	6.69	8.15	6.57
21	0.50	0.94	1.53	1.04	3.98	6.33	9.20	6.79
24	0.64	1.29	2.32	1.52	5.05	9.27	14.73	9.91
V_f : head advancement rate R_a top: average arithmetic roughness near top surface of piece R_a mid: average arithmetic roughness at mid thickness of piece R_a bot: average arithmetic roughness near bottom surface of piece R_a average: average measured R_a values R_z top: roughness on 10 extreme points near the top surface of piece R_z mid: roughness on 10 extreme points at mid thickness of piece R_z bot: roughness on 10 extreme points near the bottom surface of piece R_z average: average measured R_z values								

[0107] Two operating conditions are revealed by the test:

- a complete but irregular cut is achieved at high $v_f = 24$ mm/min;
- a high-quality cut is achieved at lower v_f , such as $v_f = 6$ mm/min is an ideal value because it minimizes the wall

taper, making it possible to use both sides of the cut given a tolerance of 1 hundredth of a millimeter, without having to introduce taper of the head to compensate for the defect.

Example 2: Complex cutting test

[0108] The new system proves to be effective in cutting thick metal sheets (at least for micro abrasive jet standards) at different levels of v_f and also in drilling with different strategies.

[0109] A complex shape is chosen for a complete characterization of the new system performance. This is the letter "A" in a particular font, used as a reference piece, as it contains:

- straight lines, where to measure roughness and streaks due to irregularities in the formation of the jet;
- acute angles, both inner and outer, to show the precision of the jet in defining the edges with a reduced jet lag effect;
- small radius curves, to show the limit of radius achievable according to the size of the jet;
- thin walls, to demonstrate the high stability and delicacy of the jet;
- long processing path, as a strength test for the stability and robustness of the system.

[0110] The smallest A which can be obtained with the focusing nozzle $d_f = 0.20$ mm and the abrasive #230 mesh, minimum jet size available on the micro AWJ market to date, is 12 mm high and has a minimum radius of 0.12 mm. For the present study, the drawing was resized to 75%, whereby reaching a final height of 9 mm and a minimum radius of 0.09 mm.

[0111] Table 2 summarizes the main processing parameters for the execution of this reference piece, cut with the disclosed cutting machine, replicating the complete execution of the cutting program three times.

Table 2: Configuration and process parameters for sample production on 2-mm thick austenitic stainless steel (AISI 301 / EN 1.4310).

Parameter / Operation	Value / Strategy
Primary nozzle diameter [mm]	0.05
Focusing nozzle diameter	0.13
Hydraulic pressure [MPa]	350
Abrasive [type and mesh]	Garnet #600 mesh
Abrasive flow rate [g/min]	3
Pressure in mixing chamber [bar]	0.78 - 0.80
Advancement rate [mm/min]	6
Drilling strategy	Circular
Drilling time [s]	4
Distance from piece being drilled [mm]	1.2
Distance from piece being cut [mm]	0.2
Cutting length [mm]	90
Cutting time [min]	15

[0112] The sample is then detached from the base material to be observed and measured. Figure 6 shows the resulting sample in a top-down view, where the precision and accuracy resulting from the cut can be observed. The sample is used to evaluate the cutting width in different cutting directions, showing no significant variation in all measurements.

Example 3: Comparison with the background art in the execution of a cut

[0113] The comparison between the abrasive water-jet cutting machine according to the invention and an abrasive water-jet cutting machine according to the background art in cutting a 2-mm thick austenitic stainless-steel sample (AISI 301 / EN 1.4310) is shown here.

[0114] The technical specifications of the abrasive water-jet cutting machine according to the invention and of the abrasive water-jet cutting machine according to the background art are listed in Table 3.1, while the results obtained

following the test are shown in Table 3.2.

[0115] As shown in Tables 3.1 and 3.2, and as shown in figure 7, the abrasive water-jet cutting machine according to the invention displays improvements compared to the prior art, in terms of the kerf quality, with cutting width reduced by 35%, and quality of roughness, with Ra and Rz reduced by 57%.

[0116] Furthermore, the abrasive water-jet cutting machine, according to the invention, achieved such results respecting the tolerance of 1 hundredth of a millimeter on the taper of the wall.

Table 3.1: Technical specifications

	Background art	Cutting machine according to the invention
Primary nozzle diameter [mm]	0.08	0.05
Focusing nozzle diameter [mm]	0.20	0.13
Hydraulic pressure [MPa]	350	350
Abrasive	Garnet	Garnet
Abrasive mesh [# mesh]	#230 mesh	#600 mesh
Distance from piece [mm]	0.35	0.20

Table 3.2: Test results

	Background art	Cutting machine according to the invention
Kerf width [mm]	0.245	0.159
Wall taper [mm]	-0.001	0.007
Roughness Ra [μm]	top 1.10; mid 1.25; bot 1.38	top 0.37; mid 0.51; bot 0.65
Roughness Rz [μm]	top 8.77; mid 8.80; bot 9.87	top 3.17; mid 3.83; bot 4.62

[0117] Of course, a person skilled in the art can make further changes and variants all contained within the scope of protection defined by the claims in order to satisfy contingent, specific needs.

Claims

1. An abrasive water-jet cutting machine (1), comprising:

- pumping means (2), fluidically connectable to a water source (3), for the generation of a pressurized water flow (4);
- a cutting head (5), comprising a primary nozzle (27), a mixing chamber (6) and a focusing nozzle (7), wherein the pressurized water flow (4) originating from the pumping means (2) is conveyed into the primary nozzle (27) of the cutting head (5) where the pressure energy of the pressurized water flow (4) is converted into kinetic energy so as to form a water jet (12), and wherein said water jet (12) is then conveyed into the mixing chamber (6);
- a dispensing system (8) of powdered abrasive material, comprising:
 - a tank (9) containing powdered abrasive material,
 - a feeding pipe (10), fluidically connecting the tank (9) to the mixing chamber (6) of the cutting head (5),
 - a dispenser (11), dispensing the powdered abrasive material contained within the tank (9) into the mixing chamber (6) by means of the feeding pipe (10);
 wherein the cutting head (5) mixes, in the mixing chamber (6), the abrasive material with the water jet (12) forming a water-abrasive material mixture jet (13), and said cutting head (5) dispenses the water-abrasive material mixture jet (13) by means of the focusing nozzle (7);
- wherein the powdered abrasive material contained in the tank (9) is homogeneously dispersed in suspension in a gelatinous water-based fluid (60); **characterised in that** the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid (60) is from 1.0 to 3.5.

2. A cutting machine (1) according to claim 1, wherein the mass ratio of the powdered abrasive material to the gelatinous water-based fluid (60) is of about 2.0.
- 5 3. A cutting machine (1) according to claim 1 or 2, wherein the particle size of the powdered abrasive material homogeneously dispersed in suspension in the gelatinous water-based fluid (60) is from #350 mesh to #600 mesh.
4. A cutting machine (1) according to any one of the preceding claims, wherein the mixing chamber (6) is substantially tubular in shape, forming:
- 10 - a front surface (14), a rear surface (15) parallel to the front surface (14), and a peripheral surface (29),
 - a front seat (16) at the front surface (14) and a rear seat (17) at the rear surface (15), wherein the front and rear seats (16, 17) are substantially cylindrical in shape,
 - a water inlet opening (18) at the front seat (16), and a mixture outlet opening (19) at the rear seat (17),
 - a jet channel (20), transverse to the front surface (14) and to the rear surface (15), and in flow communication with the front seat (16) and the rear seat (17) by means of the water inlet opening (18) and the mixture outlet opening (19).
- 15 5. A cutting machine (1) according to claim 4, wherein the jet channel (20) and the front seat (16) form a front shoulder (21) at the water inlet opening (18), and the jet channel (20) and the rear seat (17) form a rear shoulder (22) at the mixture outlet opening (19), and wherein a primary nozzle housing (23) is received inside the front seat (16), abutting against the front shoulder (21),
 wherein the primary nozzle housing (23) is substantially cylindrical in shape, and defines a front base (24) and a rear base (25), wherein the rear base (25) abuts against the front shoulder (21),
 wherein the primary nozzle housing (23) forms a primary nozzle seat (26) at the front base (24),
 wherein a primary nozzle (27) is received in the primary nozzle seat (26), and wherein the primary nozzle (27) transforms the pressurized water flow (4) originating from the pumping means (2) into the water jet (12).
- 20 6. A cutting machine (1) according to any one of the preceding claims, wherein the feeding pipe (10) is connected, at a first end (34) thereof, to the tank (9), and is connected, at a second end (35) thereof, to an injector member (36), and wherein the injector member (36) comprises an injector housing (37) and an injector nozzle (38), and the injector housing (37) forms a connection portion (39) adapted to connect the feeding pipe (10) to the injector member (36).
- 30 7. A cutting machine (1) according to one of claims 4 or 5 and according to claim 6, wherein the injector housing (37) forms a shaped channel (40) therein, adapted to receive the injector nozzle (38), and wherein the injector nozzle (38) forms an injection channel (41) therein, and an end portion (45) of the injector nozzle (38) is configured to protrude into the jet channel (20) of the mixing chamber (6), so that the injection channel (41) fluidically connects the feeding pipe (10) to the jet channel (20).
- 35 8. A cutting machine (1) according to claim 7, wherein the shaped channel (40) comprises an end portion (42) forming an air injection channel (43) which is concentric with respect to the end portion (42), and a coupling portion (61) adapted to achieve a shape coupling with the injector nozzle (38), and wherein the air injection channel (43) forms a gap (44) between the air injection channel (43) and the end portion (45) of the injector nozzle (38).
- 40 9. A cutting machine (1) according to claim 8, wherein the injector housing (37) forms an air flow channel (47) flowing into the air injection channel (43) and forming a connection seat (46), and wherein the air flow channel (47) is connected to a pneumatic conduit (48) at the connection seat (46), and wherein a valve (49) for the adjustment of the air flow entering the air flow channel (47) is arranged on the pneumatic conduit (48), and the air flow entering the air flow channel (47) is aspirated by the flow of the water jet (12) due to the Venturi effect.
- 45 10. A cutting machine (1) according to any one of the preceding claims, wherein the dispensing system (8) is provided with relief valves (56) to evacuate possible air or other gas bubbles present in the gelatinous water-based fluid (60) inside which the abrasive material is dispersed, which may introduce compressibility or cause interruptions in the feeding of the abrasive material dispersed into the gelatinous water-based fluid (60) at the cutting head (5).
- 50 11. A composition comprising a powdered abrasive material dispersed in suspension in a gelatinous water-based fluid (60), **characterised in that** the mass ratio of the dispersed powdered abrasive material to the gelatinous water-based fluid (60) is from 1.0 to 3.5, and wherein the particle size of the powdered abrasive material dispersed in suspension in the gelatinous water-based fluid (60) is from #350 mesh to #600 mesh.
- 55

12. A composition according to claim 11, wherein the mass ratio of the powdered abrasive material to the gelatinous water-based fluid (60) is of about 2.0.

5 13. A composition according to one of claims 11 or 12, wherein the average size of the powdered abrasive material granules is from 15 to 60 micrometers.

14. An abrasive water-jet cutting method, comprising the use of the composition according to one of claims 11 to 13.

10 **Patentansprüche**

1. Maschine (1) zum abrasiven Wasserstrahlschneiden, umfassend:

15 - Pumpmittel (2), welche fluidisch mit einer Wasserquelle (3) verbindbar sind, für die Erzeugung einer mit Druck beaufschlagten Wasserströmung (4);

- einen Schneidkopf (5), welcher eine primäre Düse (27), eine Mischkammer (6) und eine Fokussierdüse (7) umfasst,

20 wobei die mit Druck beaufschlagte Wasserströmung (4), welche von den Pumpmitteln (2) ausgeht, in die primäre Düse (27) des Schneidkopfs (5) geleitet wird, wo die Druckenergie der mit Druck beaufschlagten Wasserströmung (4) in kinetische Energie umgewandelt wird, um einen Wasserstrahl (12) zu bilden, und wobei der Wasserstrahl (12) dann in die Mischkammer (6) geleitet wird;

- ein Abgabesystem (8) für pulverförmiges abrasives Material, umfassend:

25 - einen Tank (9), welcher pulverförmiges abrasives Material enthält,

- ein Zufuhrrohr (10), welches den Tank (9) fluidisch mit der Mischkammer (6) des Schneidkopfs (5) verbindet,

- eine Abgabevorrichtung (11), welche das in dem Tank (9) enthaltene pulverförmige abrasive Material mittels des Zufuhrrohrs (10) in die Mischkammer (6) leitet;

30 wobei der Schneidkopf (5) in der Mischkammer (6) das abrasive Material mit dem Wasserstrahl (12) mischt und einen Mischstrahl (13) aus Wasser und abrasivem Material bildet und wobei der Schneidkopf (5) den Mischstrahl (13) aus Wasser und abrasivem Material mittels der Fokussierdüse (7) abgibt;

wobei das in dem Tank (9) enthaltene pulverförmige abrasive Material homogen in Suspension in ein gallertartiges wasserbasiertes Fluid (60) abgegeben wird;

35 **dadurch gekennzeichnet, dass** das Massenverhältnis des abgegebenen pulverförmigen abrasiven Materials zu dem gallertartigen wasserbasierten Fluid (60) 1,0 bis 3,5 beträgt.

2. Schneidmaschine (1) nach Anspruch 1, wobei das Massenverhältnis des pulverförmigen abrasiven Materials zu dem gallertartigen wasserbasierten Fluid (60) ungefähr 2,0 beträgt.

40 3. Schneidmaschine (1) nach Anspruch 1 oder 2, wobei die Partikelgröße des pulverförmigen abrasiven Materials, welches homogen in Suspension in das gallertartige wasserbasierte Fluid (60) abgegeben wird, #350 Mesh bis #600 Mesh beträgt.

45 4. Schneidmaschine (1) nach einem der vorhergehenden Ansprüche, wobei die Mischkammer (6) eine im Wesentlichen rohrförmige Form aufweist und bildet:

- eine vordere Fläche (14), eine hintere Fläche (15), welche zu der vorderen Fläche (14) parallel ist, und eine Umfangsfläche (29),

50 - einen vorderen Sitz (16) an der vorderen Fläche (14) und einen hinteren Sitz (17) an der hinteren Fläche (15), wobei der vordere und der hintere Sitz (16, 17) eine im Wesentlichen zylindrische Form aufweisen,

- eine Wassereinlassöffnung (18) an dem vorderen Sitz (16) und eine Mischungsauslassöffnung (19) an dem hinteren Sitz (17),

55 - einen Strahlkanal (20), welcher transversal zu der vorderen Fläche (14) und der hinteren Fläche (15) ist und mittels der Wassereinlassöffnung (18) und der Mischungsauslassöffnung (19) mit dem vorderen Sitz (16) und dem hinteren Sitz (17) in Strömungskommunikation ist.

5. Schneidmaschine (1) nach Anspruch 4, wobei der Strahlkanal (20) und der vordere Sitz (16) eine vordere Schulter (21) an der Wassereinlassöffnung (18) bilden und der Strahlkanal (20) und der hintere Sitz (17) eine hintere Schulter

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(22) an der Mischungsauslassöffnung (19) bilden und wobei ein Gehäuse (23) für eine primäre Düse an der vorderen Schulter (21) anliegend in dem vorderen Sitz (16) aufgenommen ist,

5 wobei das Gehäuse (23) für eine primäre Düse eine im Wesentlichen zylindrische Form aufweist und eine vordere Basis (24) und eine hintere Basis (25) definiert, wobei die hintere Basis (25) an der vorderen Schulter (21) anliegt,

wobei das Gehäuse (23) für eine primäre Düse an der vorderen Basis (24) einen Sitz (26) für eine primäre Düse bildet,

10 wobei eine primäre Düse (27) in dem Sitz (26) für eine primäre Düse aufgenommen ist und wobei die primäre Düse (27) die mit Druck beaufschlagte Wasserströmung (4), welche von den Pumpmitteln (2) ausgeht, in den Wasserstrahl (12) umformt.

15 **6.** Schneidmaschine (1) nach einem der vorhergehenden Ansprüche, wobei das Zufuhrrohr (10) an einem ersten Ende (34) davon mit dem Tank (9) verbunden ist und an einem zweiten Ende (35) davon mit einem Injektorelement (36) verbunden ist,

und wobei das Injektorelement (36) ein Injektorgehäuse (37) und eine Injektordüse (38) umfasst und das Injektorgehäuse (37) einen Verbindungsabschnitt (39) bildet, welcher dazu eingerichtet ist, das Zufuhrrohr (10) mit dem Injektorelement (36) zu verbinden.

20 **7.** Schneidmaschine (1) nach einem der Ansprüche 4 oder 5 und nach Anspruch 6, wobei das Injektorgehäuse (37) einen geformten Kanal (40) darin bildet, welcher dazu eingerichtet ist, die Injektordüse (38) aufzunehmen, und wobei die Injektordüse (38) einen Injektionskanal (41) darin bildet, und ein Endabschnitt (45) der Injektordüse (38) dazu eingerichtet ist, in den Strahlkanal (20) der Mischkammer (6) vorzustehen, so dass der Injektionskanal (41) das Zufuhrrohr (10) fluidisch mit dem Strahlkanal (20) verbindet.

25 **8.** Schneidmaschine (1) nach Anspruch 7, wobei der geformte Kanal (40) einen Endabschnitt (42), welcher einen Luftinjektionskanal (43) bildet, der in Bezug auf den Endabschnitt (42) konzentrisch ist, und einen Kopplungsabschnitt (61) umfasst, welcher dazu eingerichtet ist, mit der Injektordüse (38) eine Formkopplung zu schaffen, und wobei der Luftinjektionskanal (43) einen Spalt (44) zwischen dem Luftinjektionskanal (43) und dem Endabschnitt (45) der Injektordüse (38) bildet.

30 **9.** Schneidmaschine (1) nach Anspruch 8, wobei das Injektorgehäuse (37) einen Luftströmungskanal (47) bildet, welcher in den Luftinjektionskanal (43) strömt und einen Verbindungssitz (46) bildet, und wobei der Luftströmungskanal (47) an dem Verbindungssitz (46) mit einer pneumatischen Leitung (48) verbunden ist und wobei ein Ventil (49) für die Einstellung der Luftströmung, welche in den Luftströmungskanal (47) eintritt, an der pneumatischen Leitung (48) angeordnet ist und die Luftströmung, welche in den Luftströmungskanal (47) eintritt, aufgrund des Venturi-Effekts durch die Strömung des Wasserstrahls (12) angesaugt wird.

35 **10.** Schneidmaschine (1) nach einem der vorhergehenden Ansprüche, wobei das Abgabesystem (8) mit Überdruckventilen (56) bereitgestellt ist, um mögliche Luft- oder andere Gasblasen zu entfernen, welche in dem gallertartigen wasserbasierten Fluid (60) vorhanden sind, in welches das abrasive Material abgegeben wird, und welche eine Kompressibilität einführen können oder Unterbrechungen bei dem Zuführen des abrasiven Materials, welches in das gallertartige wasserbasierte Fluid (60) abgegeben wird, an dem Schneidkopf (5) verursachen können.

40 **11.** Zusammensetzung, umfassend ein pulverförmiges abrasives Material, welches in Suspension in ein gallertartiges wasserbasiertes Fluid (60) abgegeben wird, **dadurch gekennzeichnet, dass** das Massenverhältnis des abgegebenen pulverförmigen abrasiven Materials zu dem gallertartigen wasserbasierten Fluid (60) 1,0 bis 3,5 beträgt und wobei die Partikelgröße des pulverförmigen abrasiven Materials, welches in Suspension in das gallertartige wasserbasierte Fluid (60) abgegeben wird, #350 Mesh bis #600 Mesh beträgt.

45 **12.** Zusammensetzung nach Anspruch 11, wobei das Massenverhältnis des pulverförmigen abrasiven Materials zu dem gallertartigen wasserbasierten Fluid (60) ungefähr 2,0 beträgt.

50 **13.** Zusammensetzung nach einem der Ansprüche 11 oder 12, wobei die mittlere Größe der Körnchen des pulverförmigen abrasiven Materials 15 bis 60 Mikrometer beträgt.

55 **14.** Verfahren zum abrasiven Wasserstrahlschneiden, umfassend die Verwendung der Zusammensetzung nach einem der Ansprüche 11 bis 13.

Revendications

1. Machine de découpe à jet d'eau abrasif (1), comprenant :

- 5 - des moyens de pompage (2) pouvant être raccordés de manière fluïdique à une source d'eau (3), permettant la génération d'un flux d'eau sous pression (4) ;
 - une tête de découpe (5), comprenant une buse primaire (27), une chambre de mélange (6) et une buse de concentration (7),
 10 dans laquelle le flux d'eau sous pression (4) provenant des moyens de pompage (2) est acheminé dans la buse primaire (27) de la tête de découpe (5), où l'énergie de pression du flux d'eau sous pression (4) est convertie en énergie cinétique de façon à former un jet d'eau (12), et dans laquelle ledit jet d'eau (12) est alors acheminé dans la chambre de mélange (6) ;
 - un système de distribution (8) de matières abrasives en poudre, comprenant :
- 15 - un réservoir (9) contenant les matières abrasives en poudre,
 - une conduite d'alimentation (10) raccordant de manière fluïdique le réservoir (9) à la chambre de mélange (6) de la tête de découpe (5),
 - un distributeur (11), distribuant les matières abrasives en poudre contenues dans le réservoir (9) dans la chambre de mélange (6) au moyen de la conduite d'alimentation (10) ;
 20 dans laquelle la tête de découpe (5) mélange, dans la chambre de mélange (6), les matières abrasives avec le jet d'eau (12) pour former un jet de mélange eau-matières abrasives (13), et ladite tête de découpe (5) distribue le jet de mélange eau-matières abrasives (13) au moyen de la buse de concentration (7) ;
 dans laquelle les matières abrasives en poudre contenues dans le réservoir (9) sont dispersées de manière homogène en suspension dans un fluïde gélatineux à base d'eau (60) ;
 25 **caractérisée en ce que** le rapport massique entre les matières abrasives en poudre dispersées et le fluïde gélatineux à base d'eau (60) est compris entre 1,0 et 3,5.

2. Machine de découpe (1) selon la revendication 1, dans laquelle le rapport massique entre les matières abrasives en poudre et le fluïde gélatineux à base d'eau (60) est d'environ 2,0.

3. Machine de découpe (1) selon la revendication 1 ou 2, dans laquelle la granulométrie des matières abrasives en poudre dispersées de manière homogène en suspension dans le fluïde gélatineux à base d'eau (60) est comprise entre #350 mesh et #600 mesh.

4. Machine de découpe (1) selon l'une quelconque des revendications précédentes, dans laquelle la chambre de mélange (6) est de forme sensiblement tubulaire, formant :

- 40 - une surface avant (14), une surface arrière (15) parallèle à la surface avant (14), et une surface périphérique (29),
 - un siège avant (16) au niveau de la surface avant (14) et un siège arrière (17) au niveau de la surface arrière (15), les sièges avant et arrière (16, 17) étant de forme sensiblement cylindrique,
 - une ouverture d'admission d'eau (18) au niveau du siège avant (16), et une ouverture de sortie de mélange (19) au niveau du siège arrière (17),
 - un canal de jet (20), transversal à la surface avant (14) et à la surface arrière (15), et en communication de flux avec le siège avant (16) et le siège arrière (17) au moyen de l'ouverture d'admission d'eau (18) et de l'ouverture de sortie de mélange (19).

5. Machine de découpe (1) selon la revendication 4, dans laquelle le canal de jet (20) et le siège avant (16) forment un épaulement avant (21) au niveau de l'ouverture d'admission d'eau (18), et le canal de jet (20) et le siège arrière (17) forment un épaulement arrière (22) au niveau de l'ouverture de sortie de mélange (19), et dans laquelle un logement de buse primaire (23) est reçu à l'intérieur du siège avant (16), venant en butée contre l'épaulement avant (21),
 50 dans laquelle le logement de buse primaire (23) est de forme sensiblement cylindrique, et définit une base avant (24) et une base arrière (25), la base arrière (25) venant en butée contre l'épaulement avant (21),
 55 dans laquelle le logement de buse primaire (23) forme un siège de buse primaire (26) au niveau de la base avant (24), dans laquelle une buse primaire (27) est reçue dans le siège de buse primaire (26), et dans laquelle la buse primaire (27) transforme le flux d'eau sous pression (4) provenant des moyens de pompage (2) en jet d'eau (12).

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- 5 6. Machine de découpe (1) selon l'une quelconque des revendications précédentes, dans laquelle la conduite d'alimentation (10) est raccordée, au niveau d'une première extrémité (34) de celle-ci, au réservoir (9), et est raccordée, au niveau d'une seconde extrémité (35) de celle-ci, à un corps d'injecteur (36), et dans laquelle le corps d'injecteur (36) comprend un logement d'injecteur (37) et une buse d'injecteur (38), et le logement d'injecteur (37) forme une partie de raccordement (39) adaptée pour raccorder la conduite d'alimentation (10) au corps d'injecteur (36).
- 10 7. Machine de découpe (1) selon l'une des revendications 4 ou 5 et selon la revendication 6, dans laquelle le logement d'injecteur (37) y forme un canal profilé (40), adapté pour recevoir la buse d'injecteur (38), et dans laquelle la buse d'injecteur (38) y forme un canal d'injection (41), et une partie terminale (45) de la buse d'injecteur (38) est configurée pour faire saillie dans le canal de jet (20) de la chambre de mélange (6), de sorte que le canal d'injection (41) raccorde fluidiquement la conduite d'alimentation (10) au canal de jet (20).
- 15 8. Machine de découpe (1) selon la revendication 7, dans laquelle le canal profilé (40) comprend une partie terminale (42) formant un canal d'injection d'air (43) qui est concentrique par rapport à la partie terminale (42), et une partie d'accouplement (61) adaptée pour réaliser un couplage de forme avec la buse d'injecteur (38), et dans laquelle le canal d'injection d'air (43) forme un espace (44) entre le canal d'injection d'air (43) et la partie terminale (45) de la buse d'injecteur (38).
- 20 9. Machine de découpe (1) selon la revendication 8, dans laquelle le logement d'injecteur (37) forme un canal d'écoulement d'air (47) s'écoulant dans le canal d'injection d'air (43) et formant un siège de raccordement (46), et dans laquelle le canal d'écoulement d'air (47) est raccordé à une conduite pneumatique (48) au niveau du siège de raccordement (46), et dans laquelle une soupape (49) d'ajustement du flux d'air entrant dans le canal d'écoulement d'air (47) est agencée sur la conduite pneumatique (48), et le flux d'air entrant dans le canal d'écoulement d'air (47) est aspiré par le flux du jet d'eau (12) du fait de l'effet Venturi.
- 25 10. Machine de découpe (1) selon l'une quelconque des revendications précédentes, dans laquelle le système de distribution (8) est pourvu de soupapes de décharge (56) pour évacuer les éventuelles bulles d'air ou d'un autre gaz présentes dans le fluide gélatineux à base d'eau (60) à l'intérieur duquel les matières abrasives sont dispersées, qui sont susceptibles de présenter une compressibilité ou de provoquer des interruptions dans l'alimentation des matières abrasives dispersées dans le fluide gélatineux à base d'eau (60) au niveau de la tête de découpe (5).
- 30 11. Composition comprenant des matières abrasives en poudre dispersées en suspension dans un fluide gélatineux à base d'eau (60), **caractérisée en ce que** le rapport massique entre les matières abrasives en poudre dispersées et le fluide gélatineux à base d'eau (60) est compris entre 1,0 et 3,5, et dans laquelle la granulométrie des matières abrasives en poudre dispersées en suspension dans le fluide gélatineux à base d'eau (60) est comprise entre #350 mesh et #600 mesh.
- 35 12. Composition selon la revendication 11, dans laquelle le rapport massique entre les matières abrasives en poudre et le fluide gélatineux à base d'eau (60) est d'environ 2,0.
- 40 13. Composition selon l'une des revendications 11 ou 12, dans laquelle la taille moyenne des granules de matières abrasives en poudre est comprise entre 15 et 60 micromètres.
- 45 14. Procédé de découpe au jet d'eau abrasif, comprenant l'utilisation de la composition selon l'une des revendications 11 à 13.
- 50
- 55

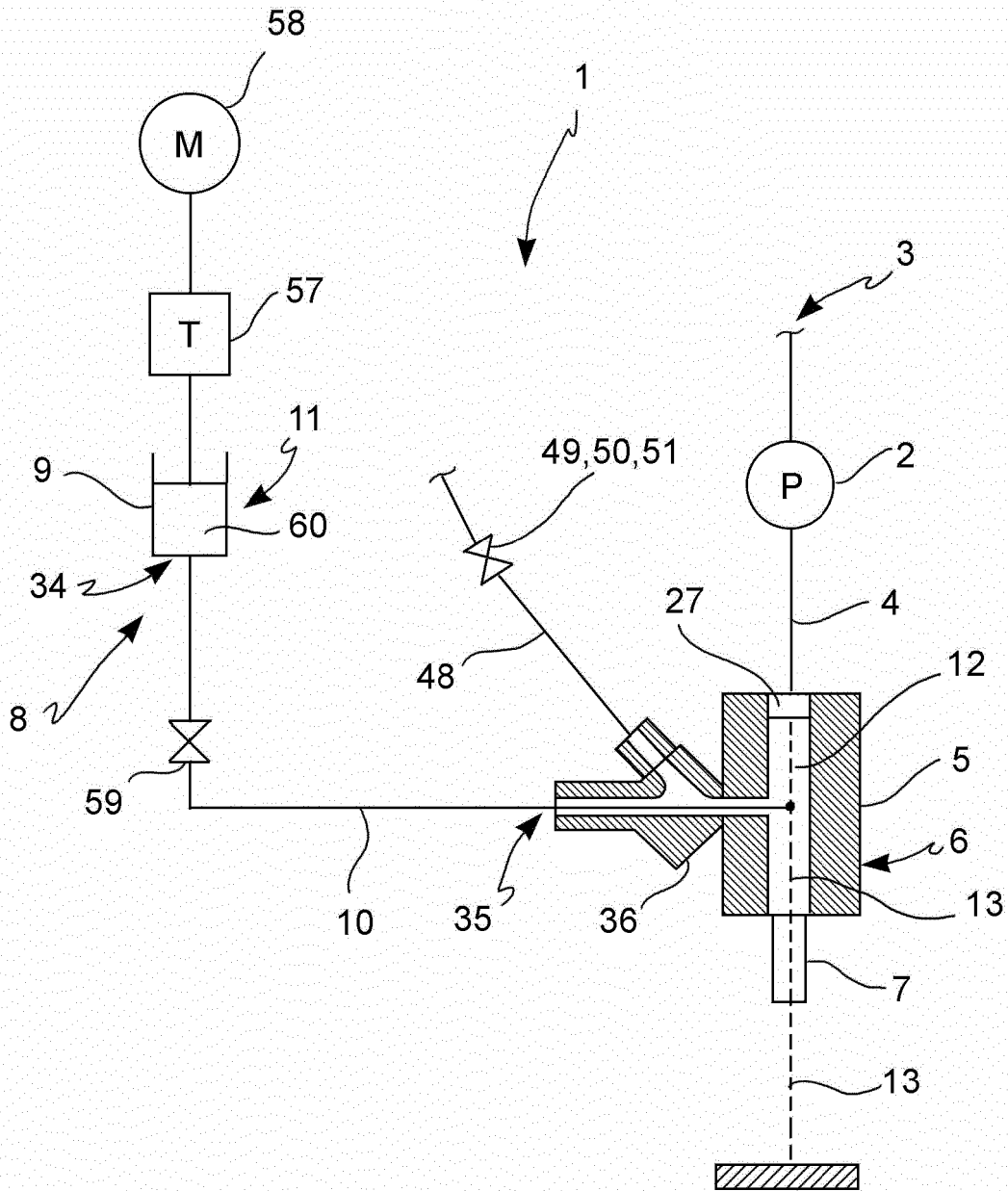


FIG. 1

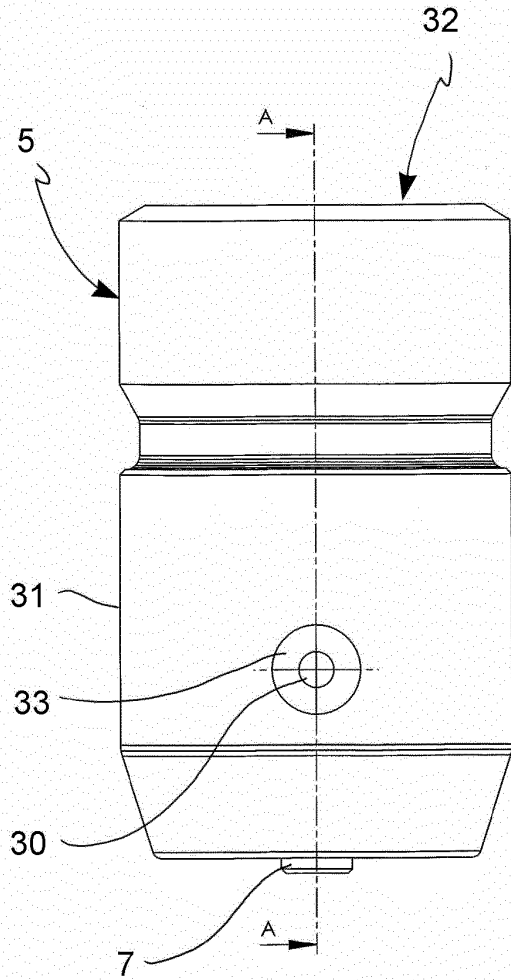


FIG. 2A

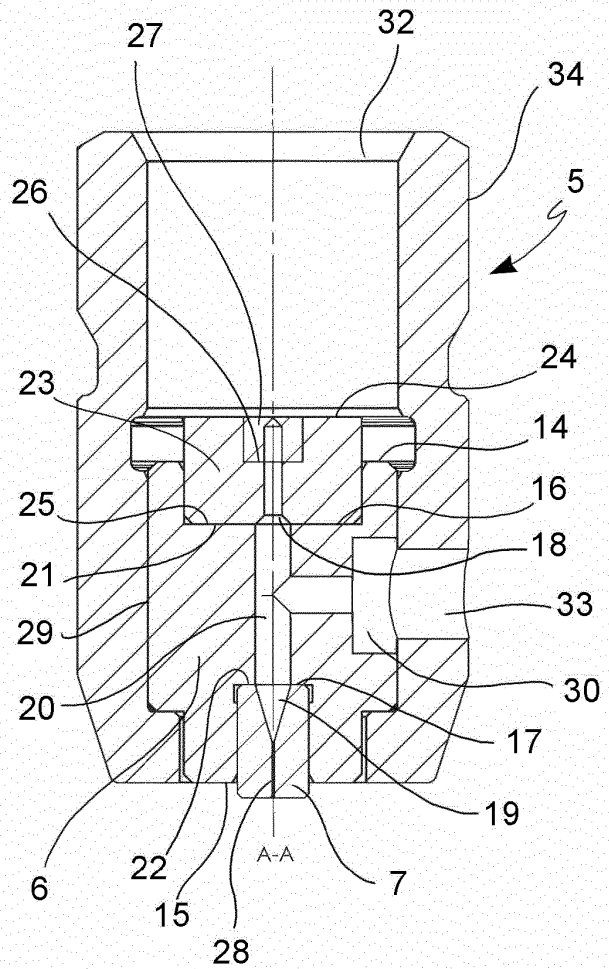


FIG. 2B

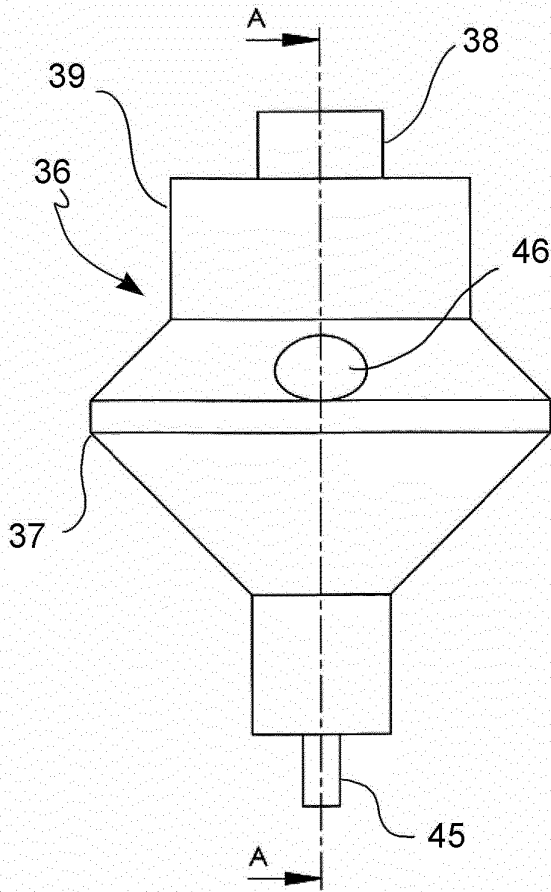


FIG. 3A

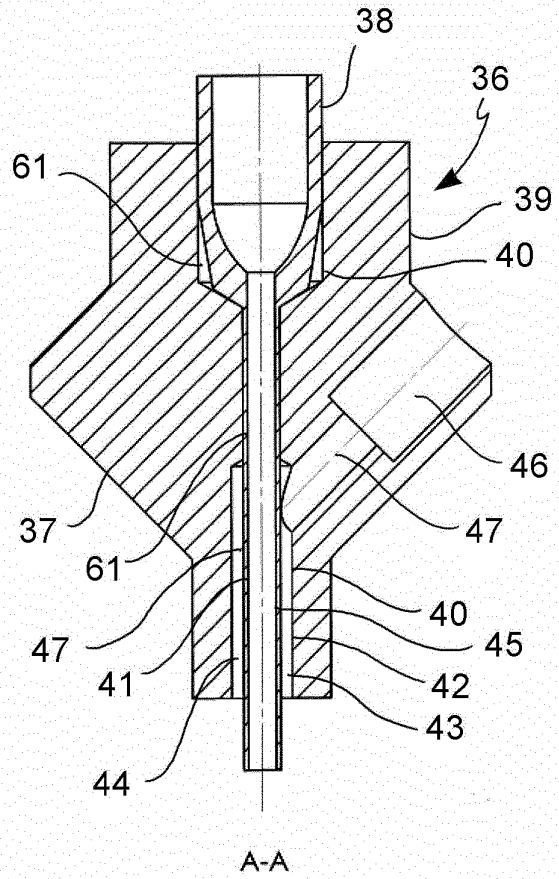


FIG. 3B

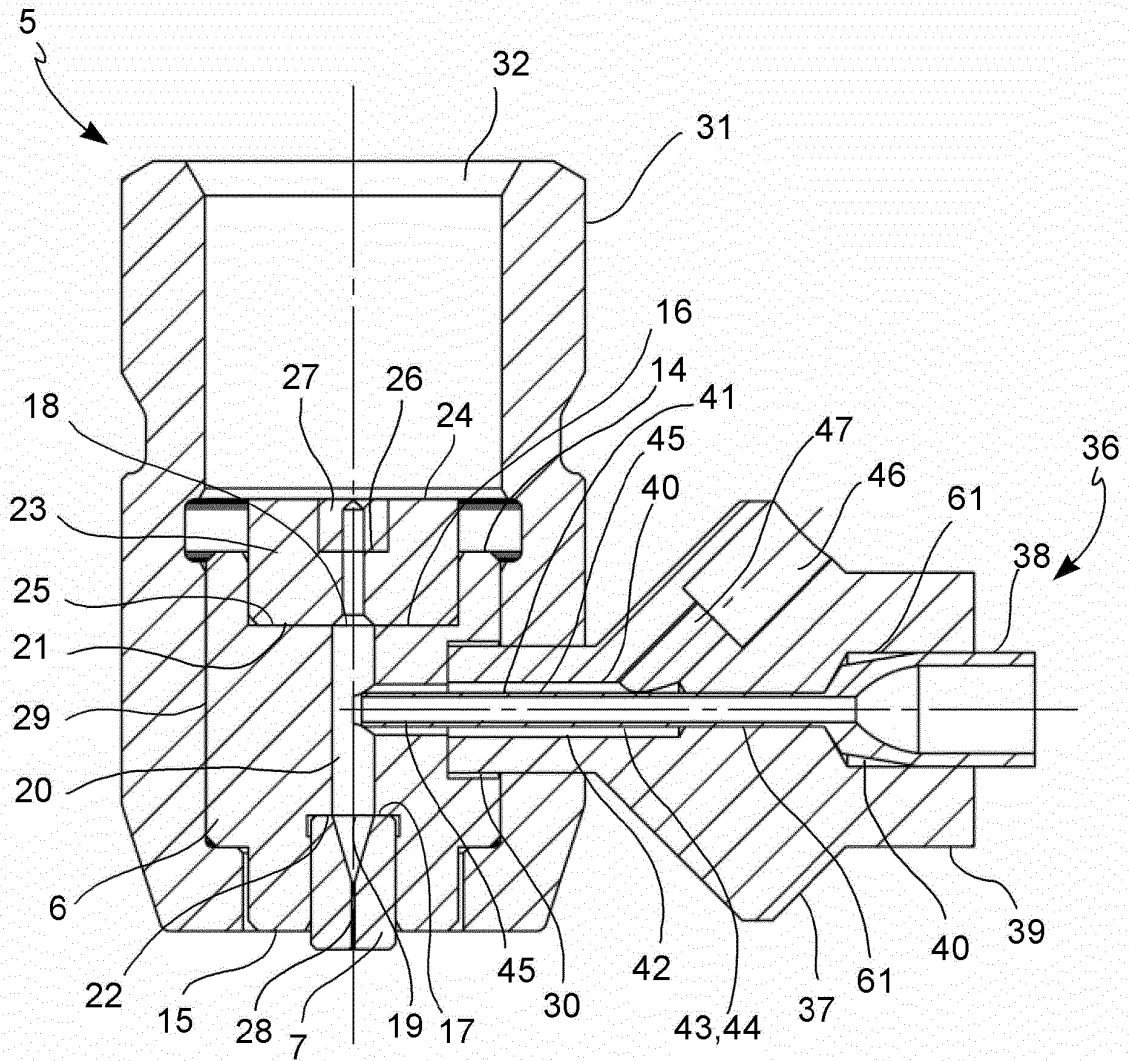


FIG. 4

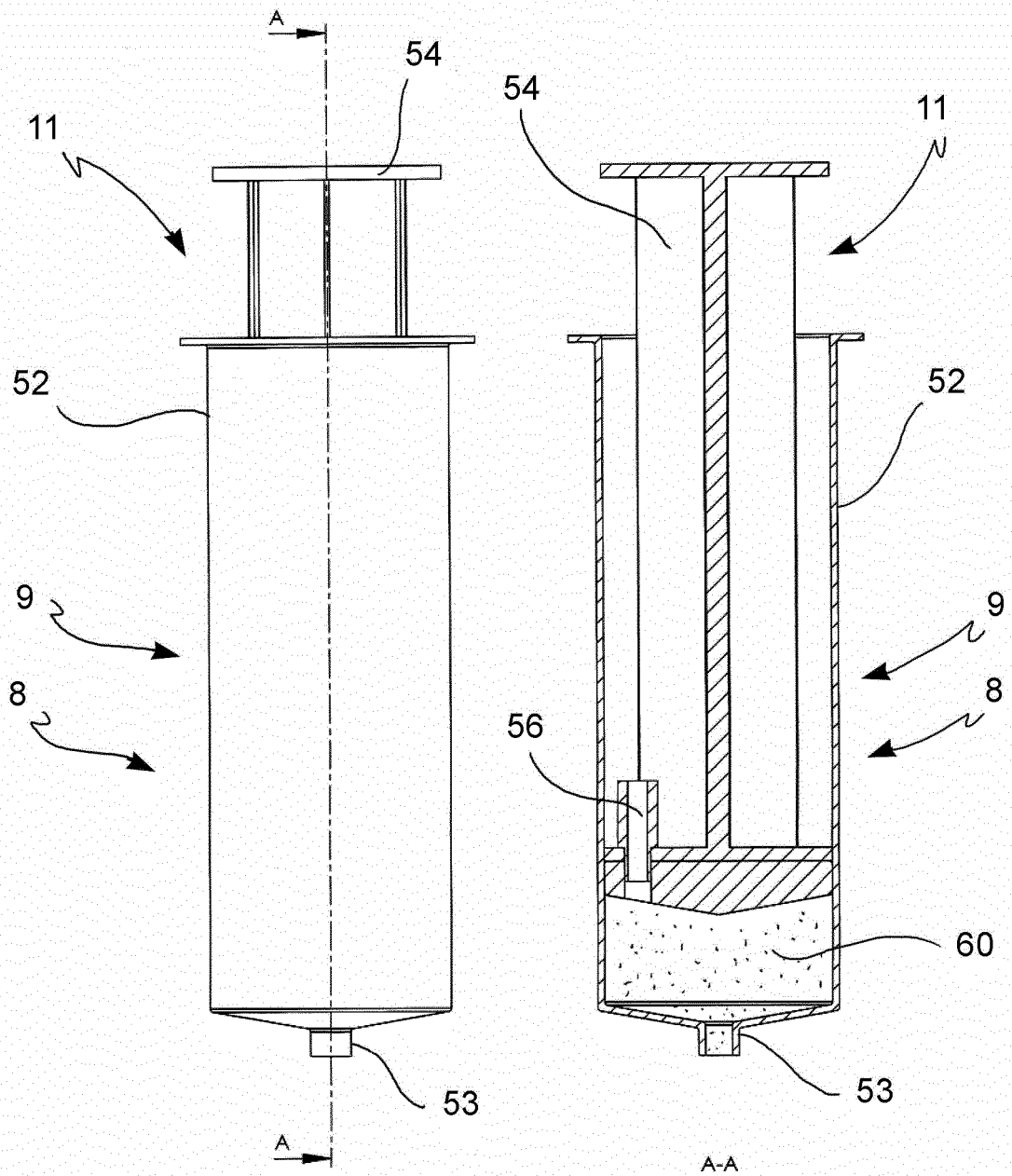


FIG. 5A

FIG. 5B

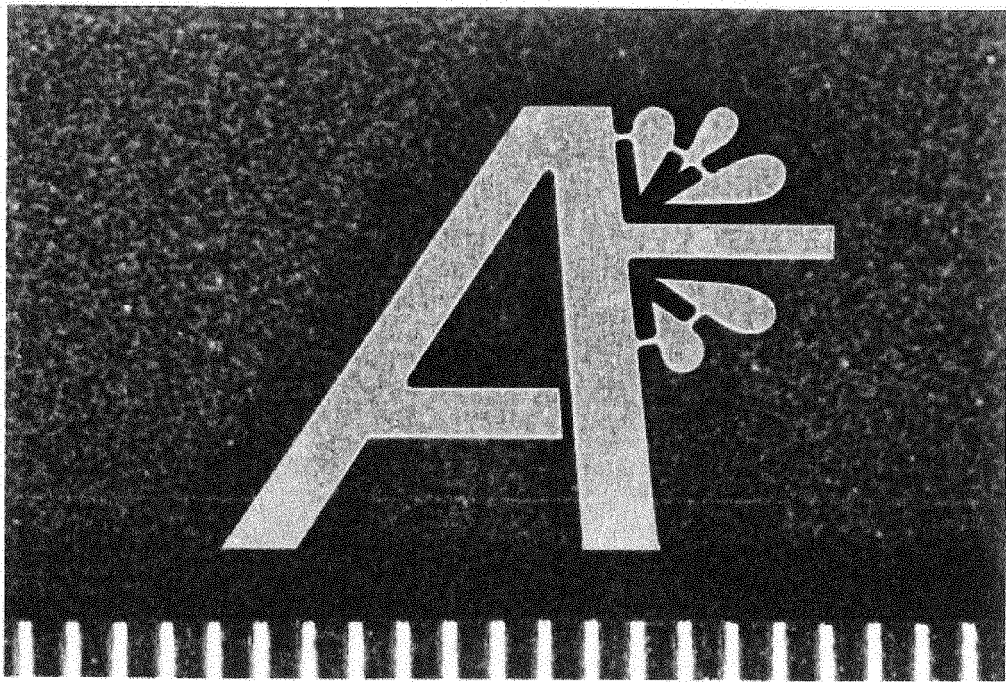


FIG. 6

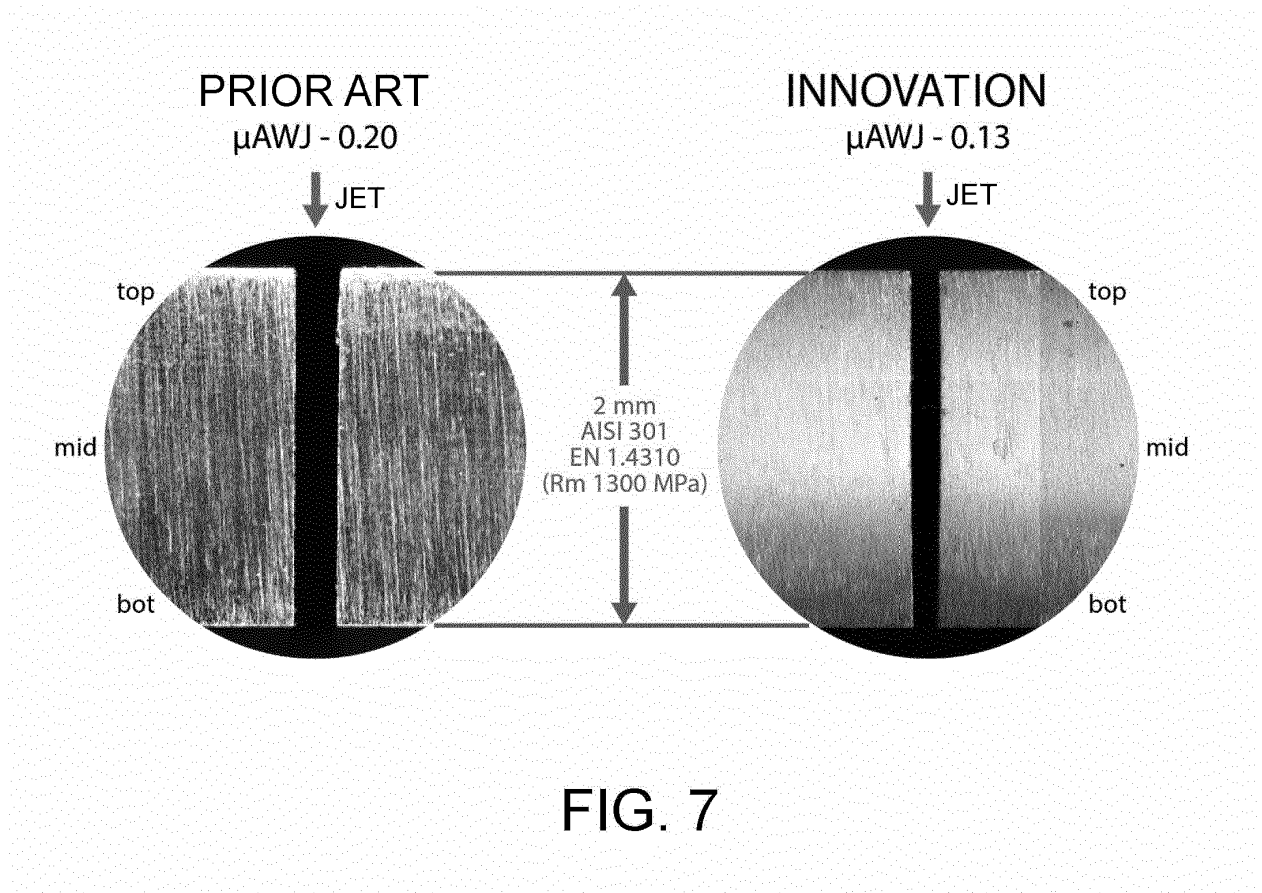


FIG. 7

REFERENCES CITED IN THE DESCRIPTION

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