

The Impact of Urban Design Elements on Microclimate in Hot Arid Climatic  
Conditions: Al Ain City, UAE.

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## 2 **Abstract**

3 Improving microclimate can be a critical consideration when designing urban places, especially in hot arid  
4 climates, due to its relation to improving human comfort in outdoor places, mitigating urban heat island effect  
5 and reducing indoors air conditioning demand. This study set out to investigate the impact of urban design  
6 strategies on microclimate, specifically canyon ratio, orientation, vegetation shading and wind speed using the  
7 case study of Al Ain City in the UAE. Simulations using Grasshopper with OpenStudio, EnergyPlus and  
8 Radiance plugins were carried out, and the Universal Thermal Climate Index (UTCI) was employed. Larger  
9 canyon ratios (1 to 2) and North-South street orientation were found to produce more comfortable urban places.  
10 While shading surfaces were found to have the potential to reduce UTCI by 5°C. Moreover, creating wind  
11 passages on the ground floor of the urban area was found to significantly enhance wind circulation in the  
12 scheme, reducing UTCI. This study can serve as an input for urban planning decision-making as well as provide  
13 guidance for urban designers in hot arid climates.

14 **Keywords:** Microclimate, universal thermal climate index, urban heat island, cooling demand, canyon geometry,  
15 urban vegetation

## 16 **1. Introduction**

17 Concern about microclimate in urban studies has increased since the 1970s (Santamouris & Asimakopoulos,  
18 2005). While climate is defined as the average atmospheric conditions over a long period of time covering a  
19 large region, the term microclimate is used to describe small-scale climate patterns over a small area that are  
20 attributed to meteorological variables (Santamouris & Asimakopoulos, 2005; Robitu, Musy, Inard & Groleau,  
21 2006; Bourbia & Boucheriba, 2010). These meteorological variables are often influenced by urban design  
22 elements, with urban geometry (urban canyon), materials and dissipation surfaces (green cover, water surfaces  
23 and soil) being the most impactful urban design elements on microclimate (Robitu, Musy, Inard & Groleau,  
24 2006; Blazejczyk et al., 2013; Perini, Chokhachian, Dong & Auer, 2017).

25 Microclimate is directly correlated with urban heat island effect (UHI), a phenomenon where urban  
26 areas air temperature is higher than the surrounding suburban and rural area. The temperature difference  
27 between rural and non-rural areas, which is known as UHI intensity, can be as high as 15°C (Santamouris &  
28 Asimakopoulos, 2005). Such increase in temperature contributes to increasing the energy consumption in  
29 buildings due to a rise in cooling demand. For instance, while a study by Salvati, Coch Roura, and Cecere  
30 (2017) estimates that 18-28% of the cooling load could be attributed to UHI, other studies reveal that this  
31 percentage could be as high as 50% (Hassid et al., 2000 Santamouris & Asimakopoulos, 2005).

32 Improving microclimate not only reduces energy consumption in buildings, but it can also reduce  
33 health issues related to heat stress as well as create more inhabitable urban spaces through increasing human  
34 comfort. This is especially important for extreme climates such as the hot arid climate of the Emirates. Initial  
35 simulation using Ladybug in grasshopper with EnergyPlus weather data file of Abu Dhabi weather station  
36 shows that there is high heat stress in more than 40% of the year (figure 5); which is defined as the periods that  
37 have above 32 °C according to (Blazejczyk et al., 2013; Bröde et al., 2012; Al Shaali, 2013)

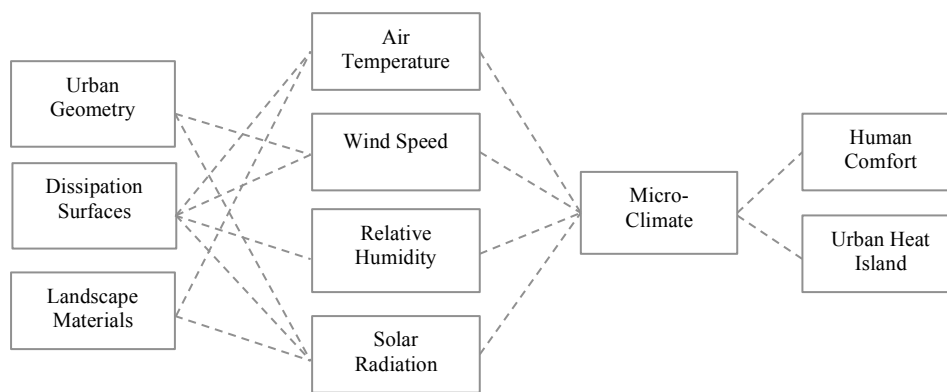
38 Despite the growing research in urban microclimate, establishing quantifiable links between urban  
39 design elements/strategies and human comfort, as represented in the Universal Thermal Climate Index (UTCI),  
40 is still an emerging field. This is especially true in climatic conditions such as that of the Emirates. Therefore,  
41 this research aims to investigate the impact of urban design strategies on microclimate in hot arid climatic  
42 conditions, using the case of Al Ain town Centre, United Arab Emirates. The main scope of this research is to  
43 determine the impact of canyon ratio, street orientation, shading surfaces and wind speed on microclimate  
44 outdoor comfort (measured with UTCI), while reflecting on the effect these strategies can have on indoors air-  
45 conditioning peak load demand.

Nomenclature	
UTCI	Universal thermal climate index
CR	Canyon Ratio
GS	Green shading surface
RH	Relative Humidity
CFD	Computational fluid dynamics
x	Air temperature
y <sub>x</sub>	UTCI at air temperature x

### 55 ***1.1 Microclimate Definition, Main Variables and Importance in Mitigating Urban Heat Island Effect***

56 Microclimate is a term used to describe small-scale pattern of climate conditions on a specific space. Four  
57 meteorological elements are used to evaluate microclimate: relative humidity (RH), wind speed, solar radiation  
58 (long wave and short wave) and air temperature. The change in microclimate from one zone to another in a  
59 small area is because each of these meteorological descriptors is influenced by certain urban design elements in  
60 the space. Lin et al., (2017) specify that the most influential urban design elements on micro climate are urban  
61 geometry, landscape materials and the presence of surfaces that dissipate heat, such as green and water

62 elements. Each of the main three urban design elements has impacts on the four meteorological descriptors of  
 63 microclimate. Urban geometry can impact the wind speed by either accelerating or buffering it. The geometry of  
 64 buildings can also trap solar radiation through multiple reflections, which influence air temperature. Moreover,  
 65 the presence of dissipation surfaces influences the saturation of air with water particles (relative humidity), as  
 66 well as impact air temperature through evapotranspiration and providing shading from solar radiation.  
 67 Meanwhile, the materials' ability to store heat (heat capacity) and reflect solar radiation (albedo) have  
 68 significant impacts on surface temperature, which in turn impacts air temperature through convection and  
 69 conduction. Figure 1 displays the connection between the main urban design elements and parameters of  
 70 microclimate.



71  
 72 Fig. 1 Urban design elements and micro-climate parameters, and their impacts on UHI and human comfort

73 UHI has been a growing concern over the last few decades due to its effect on increasing energy  
 74 consumption, climate change, as well causing heat-stress related health issues. In Athens, for example, Hassid et  
 75 al. (2000) evidenced that similar buildings (construction type and scale wise) were found to have 50% more  
 76 energy consumption in the city centre than buildings outside the city. A study by Santamouris and Georgakis  
 77 (2003) showed that the difference in temperature between urban and rural areas (UHI intensity) can reach up to  
 78 16°C. Simulations by Salvati estimate that UHI is responsible for 18-28% of the total cooling demand in Hong  
 79 Kong (Lin et al., 2017), while Akbari et al. recognized that 3-8% of electricity demand in the US is used to  
 80 compensate for UHI effect (Santamouris & Asimakopoulos, 2005). There is a wide consensus among  
 81 researchers that UHI effect is mainly attributed to the canyon effect (which traps the emitted long-wave solar  
 82 radiation and blocks wind circulation), loss of dissipation surfaces (green and water surfaces), hardscape  
 83 materials (low albedo and high latent heat storage capacity) (Giridharan, Lau, & Ganesan, 2005). It is clear that  
 84 the variables that impact the microclimate are the same ones that control the UHI effect, which means that the  
 85 accumulating effect of improving microclimate in multiple urban places would not only create more  
 86 comfortable urban places, but also significantly contribute to mitigating the UHI effect.

87 ***1.2 The Impact of Urban Design Elements on Microclimate: Urban Vegetation***

88 Urban vegetation is a major urban design tool in regulating microclimate. In cooler climates, it serves as a buffer  
89 of undesirable wind when oriented correctly (Lin et al., 2017), and in hotter climates it reduces air temperature  
90 through evapotranspiration, shading and direction of wind (Lemes de Oliveira, 2017). Trees are found to be  
91 more effective in improving microclimate than grass due to their higher transpiration rate and their shading  
92 effect (Santamouris & Asimakopoulos, 2005). Furthermore, Perini and Magliocco (2014) estimate that  
93 vegetation has an albedo (ability to reflect long-wave solar radiation) of 0.2-0.3, which is much higher than  
94 hardscape surfaces like asphalt, with albedo of 0.05. This adds to vegetation's ability to improve the  
95 microclimate. They also recognized that the hotter the climate the more impactful vegetation becomes in  
96 reducing temperature, which have been shown to range from 2-3 °C in Mexico City (Jauregui, 1990) to 2-8 °C in  
97 Los Angeles (Taha et al., 1991).

98 ***1.3 The Impact of Urban Design Elements on Microclimate: Canyon Geometry***

99 Canyon geometry is a term introduced by Oke in 1981 to relate the building height, street width and its length to  
100 each other (Lin et al., 2017). Studying the relationship between canyon geometry and the microclimate has been  
101 the subject of several researches, which attempted to specify the ideal height to street width ratio from a  
102 microclimate perspective (Toudert, & Mayer, 1997; Johansson, 2006; Giannopoulou, 2010). Some researchers  
103 also add street orientation to the variables (Toudert & Mayer, 1997; Taleb & Abu-Hijleh, 2013). The ideal  
104 canyon ratio recommended by such studies changes based on the climatic context of each area. Oke suggested,  
105 for instance, that an ideal height (H) over width (W) ratio is 0.4- 0.6 for mid-latitudes ( $H/W = 0.4$  to  $0.6$ ). A  
106 study conducted in Athens in 2010 support these ratios, which concluded that the lower the ration the better the  
107 cooling (Giannopoulou, 2010). The enhanced cooling could be explained by the increased ventilation due to the  
108 wide distances between buildings, where wind is not blocked by compacted urban form. The large distances  
109 between buildings also mean that multiple reflections of the incoming short-wave solar radiation, and the re-  
110 emitted long-wave radiation are less likely, and therefore trapped heat carried by both long and short-wave solar  
111 radiation is reduced.

112 On the contrary, Johansson's study in Fez, Morocco (2006) shows that better cooling is achieved  
113 through higher ratio (more compact form) than the discussed above, which is supported by a previous study in  
114 Ghardaia, Algeria with similar climate (Toudert, & Mayer, 1997). This indicates that a more compacted urban  
115 form with deeper canyons would be desired. There could be several explanations for these contradictory  
116 recommendations. While a compact urban form tends to trap heat and block wind ventilation, it also often

117 presents higher shading factors. Therefore, it seems likely that in Fez and Ghardaia, the shading factor is more  
118 effective as a cooling strategy than wind ventilation. In turn, in Athens wind ventilation seems to be more  
119 critical than sun shading when it comes to reducing air temperature. This could be attributed to the differences in  
120 climate characteristics. Although the three cities are in mid-latitudes, Athens' climate is less dry and slightly  
121 cooler than Fez and Ghardaia. In Dubai, an urban configuration that allows for better wind circulation (organic  
122 configuration) was found to reduce air temperature by more than 0.5°C (not the UTCI temperature) compared to  
123 a less permeable configuration (orthogonal) (Taleb & Abu-Hijleh, 2013).

#### 124 ***1.4 Universal Thermal Climate Index (UTCI)***

125 UTCI temperature is not only dependent on the environmental conditions (meteorological variables), but also on  
126 gender, body mass, physical activity as well as clothing level. All these variables impact the human thermo-  
127 physiological response (Blazejczyk et al., 2013). Consequently, in 2000, the International Society of  
128 Biometeorology formed a commission for establishing a quantity to identify human perception of temperature  
129 (Bröde, n.d.). In 2009, the international and multidisciplinary group of experts in thermo-physiology,  
130 physiological modeling, meteorology and climatology developed the Universal Thermal Climate Index (UTCI).  
131 It is a one-dimensional quantity that measures human psychological response to actual thermal conditions,  
132 which is determined by multidimensional variables. The quantity is supposed to be valid for all climatic  
133 conditions, seasons and genders (Blazejczyk et al., 2013; Bröde et al., 2012; Jendritzky, de Dear & Havenith,  
134 2012). This means that a UTCI of 24°C would feel the same in the United Kingdom as it does in Morocco or in  
135 Brazil. UTCI model takes the input variables of wind speed, relative humidity, air temperature, mean radiant  
136 temperature, clothing level (measured by clo) and metabolic rate (MET) and calculate an equivalent temperature  
137 that considers these variables. The matrixes involved in the UTCI accounts for the differences caused by gender,  
138 age and weight (Bröde et al., 2012).

#### 139 **2. Methodology**

140 In order to access the impact of canyon ratio, canyon orientation, shading by vegetation, and wind speed on  
141 Microclimate comfort; simulation using EnergyPlus and Open Studio was carried out. The results of the both  
142 simulations were combined and visually presented using Grasshopper. This integrated modelling approach  
143 allows for estimating the impact of building materials on micro-climate comfort as well as energy consumption.  
144 The simulation was implemented in The Town Square of Al Ain City. UTCI has been used as the descriptive  
145 quantity for microclimate and comfort maps have been produced for the different conditions. Moreover, to

146 estimate one possible impact of changing the urban design elements on energy consumption, simulation of the  
147 peak air conditioning demand throughout the year was conducted.

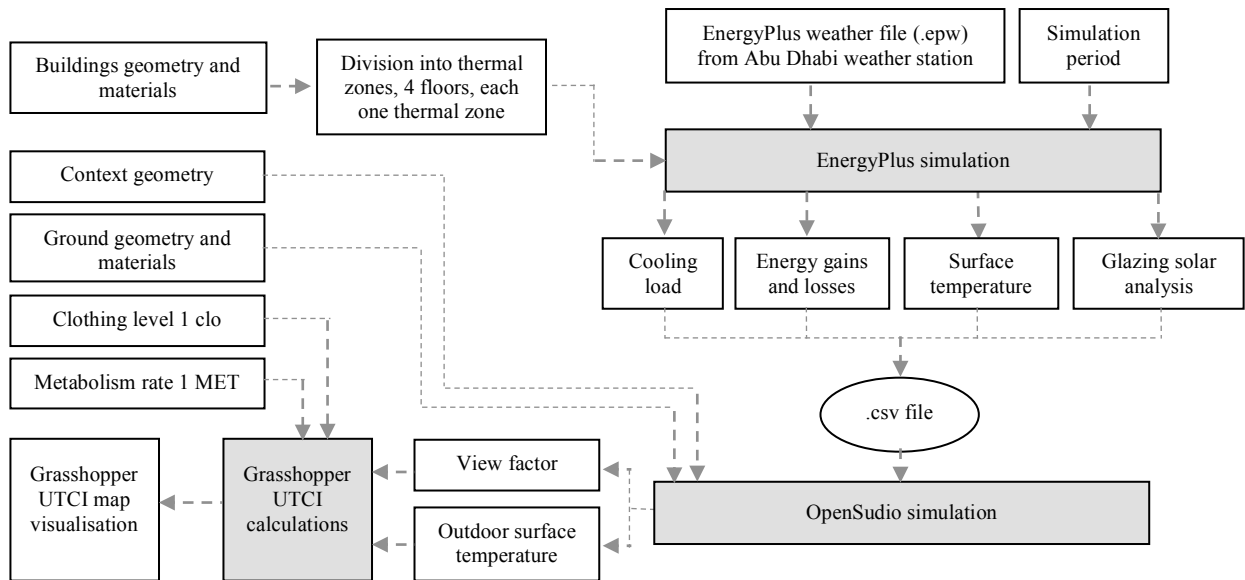
## 148 ***2.1 Simulation Model and Algorithm***

149 Figure 2 displays the software simulation model and the main inputs and outputs. EnergyPlus and OpenStudio,  
150 integrated with Grasshopper, were used to produce the UTCI comfort maps and air conditioning peak load  
151 demand. First, the canyon geometry and materials were created in Grasshopper (table 1) and divided into  
152 thermal zones (floors). The building characteristics and the analysis period, along with the meteorological  
153 variables (Wind speed, mean radiant temperature MRT, Air temperature, relative humidity) that have been  
154 extracted from Abu Dhabi weather station data file (.epw), has been input into EnergyPlus. EnergyPlus allows  
155 for layer-by-layer simulation of energy transfer through buildings' construction materials (EnergyPlus, 2018). It  
156 has been used in this study to simulate the peak required cooling demand for the buildings, energy gains and  
157 losses, indoor surface temperature, and the solar analysis of the glazing. The results of the simulation have been  
158 extracted in the form of .csv and imported into OpenStudio, where advance daylight assessment is included to  
159 simulate the outdoor surface temperature, including the outdoor context geometry and shading surface. This  
160 advanced daylight assessment also simulates the view factor, which is a necessary input to calculate and  
161 visualise UTCI in Grasshopper through its Outdoor Comfort Calculator Component.

162 Open Studio is a software that allows for whole building energy modeling through inclusion of  
163 advanced daylight analysis. It has been developed by the US Department of Energy and the National Renewable  
164 Energy Laboratory, and its validity has been supported by several articles (Roth, Brackney, Parker, & Beitel,  
165 2016; Macumber, Ball, & Long, 2014). EnergyPlus has been verified by multiple published articles, including  
166 ASHRAE journal (Crawley, Lawrie, Pedersen & Winkelmann, 2000). Grasshopper Outdoor Comfort Calculator  
167 Component (in Ladybug Plug-in), where UTCI values are calculated and visualized, uses the source code of the  
168 equations developed by The International Society of Biometeorology in attempt to quantify human comfort  
169 through UTCI (Matzarakis, Mayer, Chmielewski, 2010; Jendritzky, Havenith, Weihs, Batschvarova, & DeDear,  
170 2008; Perini et.al., 2017). Grasshopper is an algorithm-based plug-in for Rhinoceros. It allows users with no  
171 coding experience to manage, manipulate and visualize data through its visual interface. Figure 2 shows a  
172 diagram of the implemented tools, and figure 3 displays a portion of the simulation Algorithm in Grasshopper.

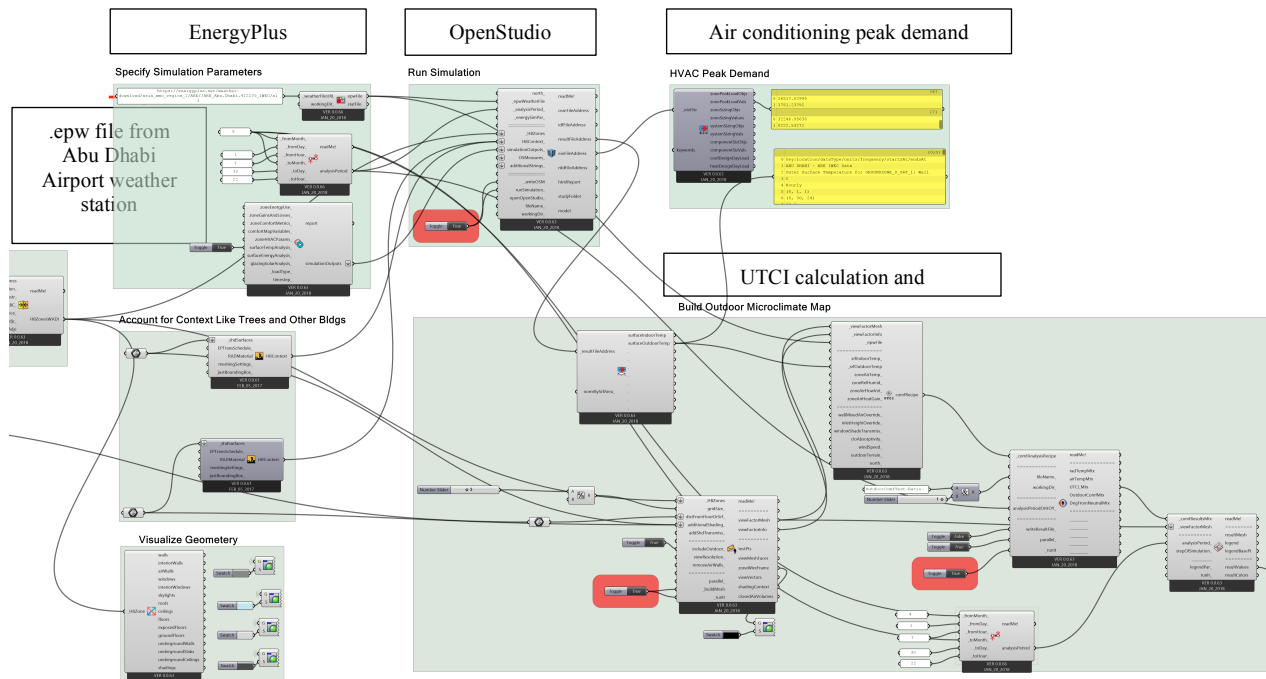
173 Several researchers have generated micro-climate comfort maps using Grasshopper (Perini et.al., 2017;  
174 Chokhachian, Santucci & Auer, 2017); however, they used TRNSYS as the simulating tool for energy transfer

175 through building construction, and ENVI-Met to account for computational fluid dynamics (CFD) and  
 176 vegetation. Both software performances are well verified. In this paper, a clothing level of 1 clo (a three-piece  
 177 suit) was used as a constant in the comfort simulations, which is an assumption that is based on mild winters and  
 178 that the clothing level in summer does not decrease due to the conservative culture of the city. A metabolic rate  
 179 of 1 Met was assumed since leisure activities (slow walking and sitting) are targeted in the town square.



180

181 Fig.2 Diagram of the implemented software model with the main inputs and outputs



182



183 Fig.3 A portion of the algorithm in Grasshopper showing the integration of EnergyPlus with OpenStudio and the  
184 extraction of the simulation meteorological outputs into the UTCI calculator. Full script is available in data in  
185 brief, figure 1.

## 186 **2.2 UTCI Model**

187 The matrices and equations used inside the UTCI calculator in grasshopper are based on the equations from the  
188 UTCI-Fiala model. This is done through, first, modeling the heat exchanges within the body. Second, modeling  
189 the heat exchanges between the surface temperature of the body and the surrounding environment. Third,  
190 measuring the thermoregulatory reaction of the central nervous system and the perceptual response (Fiala,  
191 Havenith, Bröde, Kampmann, Jendritzky, 2012).

192 The calculations of the heat exchanges within the body includes three exchanges; the dynamic heat transfer  
193 within the body systems using Bioheat Transfer equation. This includes variables such as Arterial blood  
194 temperature and Tissue temperature. The second internal heat exchange is due to the resultant heat from blood  
195 circulation. While the third heat exchange within the body is the Metabolic Heat Production (Fiala, Havenith,  
196 Bröde, Kampmann, Jendritzky, 2012). These equations are calculated in the UTCI calculator in grasshopper  
197 based on the input data of metabolic rate and clothing level (1 MET and 1 clo in this research).

198 The EnergyPlus in Grasshopper simulate the resultant meteorological conditions that are impacted by the  
199 context variables; where the input meteorological data from .epw file are analyzed in the new context. These  
200 meteorological variables (Wind speed, mean radiant temperature MRT, Air temperature, relative humidity) are  
201 impacted by the Canyon ratio, orientation, the construction materials of the surrounding buildings and ground,  
202 and the vegetation shading elements (Milošević, Bajšanski, Savić, & Žibera, 2016, p.25), and in (Roudsari,  
203 Pak, Smith, 2013). The new meteorological conditions are then used in the UTCI calculator to model the heat  
204 exchanges between the surrounding environment and body surface temperature; which has been calculated  
205 based on the metabolic rate and clothing level.

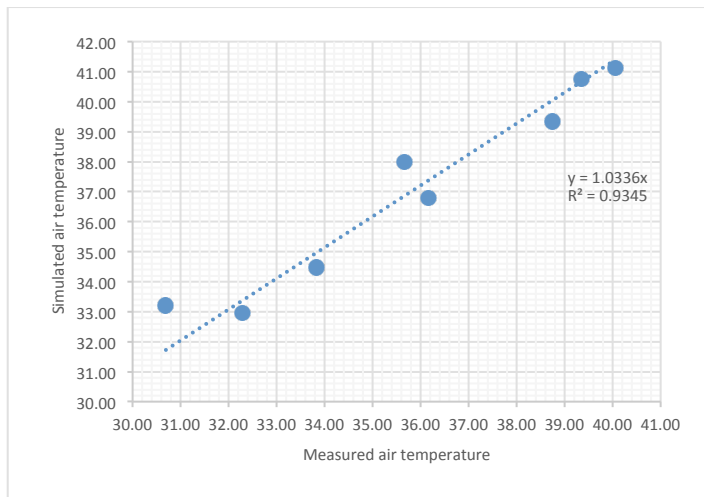
206 Finally, a thermoregulatory system equations are used to calculate the psychological responses of different  
207 conditions. This system measures the thermoregulatory responses of the human central nervous system to  
208 different conditions of transient, cold stress, cold, moderate, warm, and hot stress, in comparison with the steady  
209 state, as well as under different activity levels (up to heavy exercise), and actual sense of temperature values has  
210 been assigned (UTCI values). This system has been developed through physiological experiments (Fiala,  
211 Havenith, Bröde, Kampmann, Jendritzky, 2012).

### 212 **2.3 Model Validation**

213 In order to validate the Software simulation, a similar validation approach to Perini et.al. (2017) has been  
214 adopted. The field measurements of air temperature from Abu Dhabi weather station has been compared to the  
215 simulated air temperature of the model using EnergyPlus and OpenStudio combination in Grasshopper (data in  
216 brief, table 1 and figure 2). Abu Dhabi weather station is located at 24°43' N, 54°65' E, and on an elevation of  
217 27m (Weather Data Download - Abu Dhabi 412170, n.d.). The average measured hourly air temperature from 7  
218 AM to 10 PM in August was compared to the average hourly simulated air temperature for the same period. The  
219 simulation was conducted on the no vegetation scheme with canyon ratio of 1, and at 1.6 m (human level).

220 It appears that the simulated values are very comparable to the field measurement ones, with an average error of  
221 1.95% (average absolute error of 1.23 C°) between the measured and simulated results at every hour. Higher  
222 accuracy is noticed at lower temperatures during night time (figure 4), where the software seems to overestimate  
223 the actual temperature. The measured data is at 27 m altitude, while the simulated data is at 1.6 m height (human  
224 level in the tests). The model simulates the ambient temperature in the context of the study with surrounding  
225 buildings that has the construction materials of table 1 and canyon ratio 1. Therefore, the main different  
226 variables between the simulated and measured data are the presence of shading elements, blocking the wind  
227 profile, the stored heat in the thermal mass of the buildings in the simulated case, and long wave radiation.  
228 These elements in the simulated case should contribute to increasing the ambient temperature, with the  
229 exception of the shading elements that can reduce the temperature. This could be an interpretation of why the  
230 simulated hourly ambient temperature is slightly higher than the measured one (data in brief, figure 2 and table  
231 1). The graph shows that at evening hours the simulated temperature is very close to the measured data, which  
232 can be attributed to less differences in the variables between the simulated and measured data.

233 The low discrepancy between the measured and simulated data suggests a high validity of the simulation  
234 method.



235

236 Fig.4 Validation of the simulation model. Low discrepancy between the simulated air temperature and the  
 237 measured air temperature indicates a high validity of the model.

#### 238 **2.4 Test Period**

239 April, August and December were selected to represent three different conditions of the year: moderate heat  
 240 stress (26-32 °C, which is in April, May, October, November), extreme heat stress (above 32 °C, in June, July,  
 241 August, September) and no heat stress (9-26 °C, in January, February, March, December). This has been  
 242 assessed based on the data from EnergyPlus weather file (.epw) of Abu Dhabi weather station, visualized in  
 243 Climate Consultant and Grasshopper (Ladybug, figure 5), and using the assessment of air temperature ranges by  
 244 (Blazejczyk et al., 2013; Bröde et al., 2012; Al Shaali, 2013). It is possible to bring the hours that falls in the  
 245 moderate heat stress range to comfort through passive strategies (Blazejczyk et al., 2013; Al-Shaali, 2013), and  
 246 mitigate the high heat stress hours, where 43% of the hours have a risk of high heat stress (Figure 5). The  
 247 simulations were averaged for each of the three months (April, August, December) for the period between 7:00  
 248 AM and 10:00 PM, which is the assumed occupation period of public spaces in the city centre of Al Ain (a  
 249 mixed-use area). A similar testing approach of using a continuous test period is performed by (Taleb & Abu-  
 250 Hijleh, 2013; Perini et.al., 2017).

#### 251 **2.5 Test Variables and Simulation Limitations**

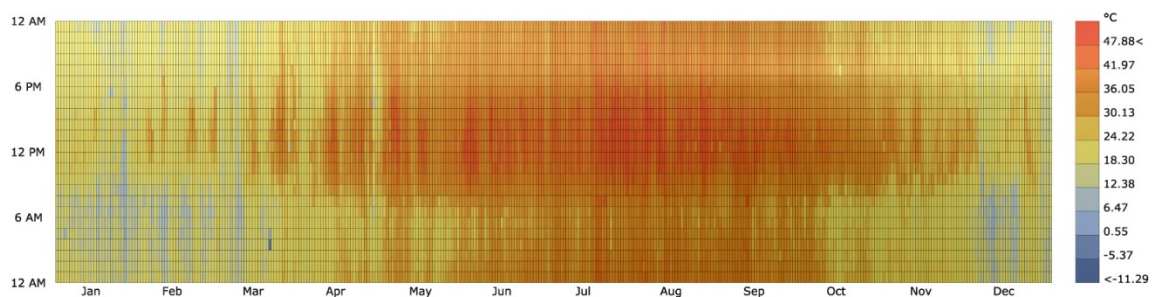
252 In order to understand how much wind speed can impact UTCI in a moderate heat stress range under constant  
 253 relative humidity, mathematical modeling of the impact of different wind speeds (between 0 m/s to 10 m/s) on  
 254 UTCI from 26°C to 32°C were conducted. The wind speed range was selected based on the initial assessment of  
 255 climate characteristics of the area using Climate Consultant Software, where the dominant wind speed range  
 256 was found to be between 2.5 m/s and 6 m/s (data in brief article, figure 4). These values fall within Lawson

257 criteria for pedestrian comfort levels, where the range is 0 m/s to 10 m/s (Pedestrian Wind Comfort Analysis  
258 Report, 2016). Air conditioning peak load estimation was performed using EnergyPlus ideal air loads air  
259 system. This assumes 100% efficiency in removing heat and humidity from outdoor air to the requirement of the  
260 indoors. It does not consider the energy loss through heat transfer in air/water loops of the air conditioning  
261 system. While it is sufficient for the purpose of the study in quantifying how much urban design strategies  
262 impact the peak demand, it should not be used as design reference for air conditioning systems. The actual peak  
263 energy demands are expected to be higher.

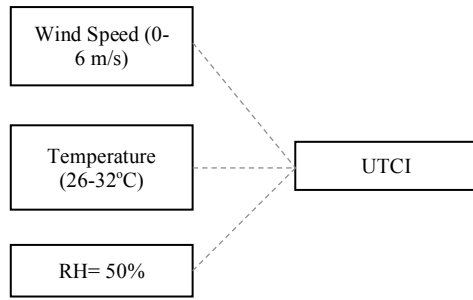
264 Additionally, the simulation considered basic wind flow using wind speed from the Abu Dhabi epw.  
265 weather data file. It does not consider the complex computational fluid dynamics (CFD) in the analysis that  
266 would be influenced by geometry. For more accuracy, CFD component could be integrated in Grasshopper or,  
267 alternatively, ENVI-MET software could be used. Another limitation of the study is that a 1 clo level has been  
268 assumed for both the cool and hot months to simplify the simulation, and due to lack of studies concerning the  
269 local subjective thermal comfort and UTCI. An experimental field study of UTCI, such as the one performed by  
270 (Bröde et al., 2012) in Brazil as well as in Canada and Korea (Park, Tuller, & Jo, 2014), can be valuable in  
271 relating UTCI to the local subjective thermal comfort in the region.

272 Figure. 6 and 7 display the tests variables. First, the impact of canyon ratio was investigated through  
273 testing three canyon ratio (CR) configurations (0.5, 1 and 2 CR). Second, testing north-west, and south-east  
274 orientations was carried out. Third, the impact of shading by vegetation has been tested through comparing 16%  
275 and 32% effective shading surfaces with no shading configuration. Finally, the wind speed impact on UTCI was  
276 assessed using UTCI calculator in Grasshopper [developed by the International Society of Biometeorology in  
277 (Matzarakis, Mayer, Chmielewski, 2010; Jendritzky, Havenith, Weihs, Batschvarova, & DeDear, 2008; Perini  
278 et.al., 2017), by plotting wind speeds from 0.1 m/s to 6 m/s (the range of wind speed at the case study location  
279 according to Abu Dhabi weather station) against UTCI temperature. Which is conducted at constant relative  
280 humidity of 50% for every air temperature increment between 26-32°C (the moderate heat stress range).

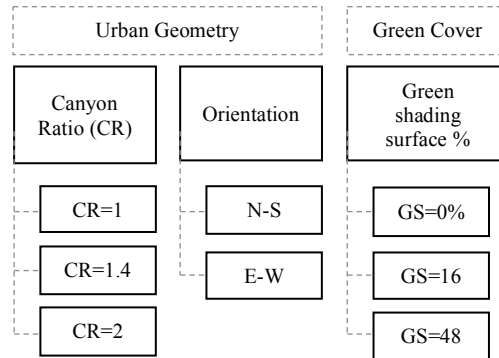
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282 Fig.5 UTCI in Al Ain/ Abu Dhabi generated using Ladybug, Grasshopper, 43% of the hours have a risk of high  
 283 heat stress.



284 Fig.6 Modelling of the impact of wind  
 285 speed on UTCI under constant RH.



286 Fig.7 Tested urban design strategies in Al

287 **3. Contextual Analysis**

288 The city of Al Ain is located at 24.1302° N, 55.8023° E, and characterized by a sprawled urban fabric, which is  
 289 to some extent a result of the lack of large-scale urban planning at the beginnings of the city's development,  
 290 since Abu Dhabi (the main political region) Urban Planning Council was only founded in 2007. Moreover, the  
 291 city has a policy of maximum allowed building height of four stories plus the ground floor, instilled by the  
 292 founder of the country Sheik Zayed in order to preserve the city's cultural value (Yildirim & El-Masri, 2010).  
 293 See Figures 8, 9 and 10 for the town square neighbourhood urban characteristics. As for the building  
 294 characteristics, Figure 11 and table 1 display the buildings' geometry and materials in the town square, which  
 295 have been used to build the model for simulation.



294 Fig.8 Al Ain town square street widths



295 Fig.9 Al Ain town square, functional distribution



Fig.10 Al Ain town square, building heights

Table.1 Buildings construction materials

Construction Element	Construction Layers	u-value
Exterior wall	100 mm brick/ cladding	0.459
	200 mm concrete block	
	50 mm insulation board	
	Air space	
	19 mm Gypsum board	
Window	3 mm clear panel	2.369
	13 mm air space	
	3 mm clear panel	

<b>Roof</b>	100 mm lightweight concrete Ceiling air space Acoustic tile	1.449
<b>Ground (external) floor</b>	50 mm insulation board 200 mm heavy weight concrete	0.556

296



297

298 Fig.11 Buildings geometry in the town square

299 **4. Results and Discussion**

300 **4.1 The Impact of Canyon Ratio on Microclimate**

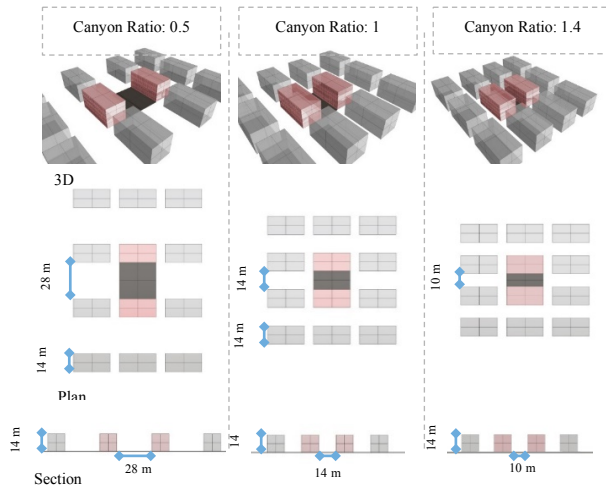
301 In order to assess how much canyon geometry impact the microclimate comfort and energy consumption in  
302 buildings in Al Ain/ Abu Dhabi climate, a simplified model was created based on the contextual analysis. Four-  
303 story buildings are found to be the most common in Al Ain central district, therefore building heights of 14 m  
304 are used (3.5 m for each floor, ignoring slab thickness and parapet height). Street widths range from 7 to 35 m  
305 inside the neighbourhood and 50 to 55m outside. Therefore, street widths of 10, 14 and 28 m are tested to cover  
306 the different ranges and determine which is the most favourable ratio (Figure 12). Higher street widths are not  
307 included in this simulation due to the insignificant impact of buildings on each other at such large distances  
308 (decided based on a preliminary simulation). Table 2 summarizes the main simulation variables.

309 Table.2 Constant variables in the simulation of the impact of canyon geometry on microclimate

<b>Street Orientation</b>	<b>East-West</b>
---------------------------	------------------

<b>Glazing percentage of the long façade</b>	30%
<b>Trees/ shading elements</b>	None
<b>Air-conditioning</b>	Ideal air flow
<b>Ground material</b>	Asphalt
<b>Buildings materials</b>	Refer to table.1
<b>Simulation height from the ground</b>	1.5 m

310



311

Fig.12 CR tests geometry

312

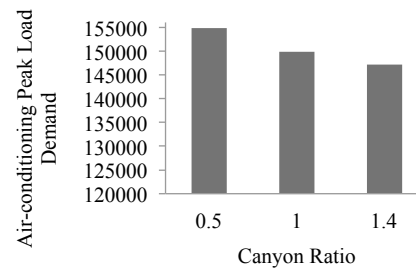


Fig.13 Air conditioning vs. canyon ratio

313 Figure.14 displays the outdoor microclimate comfort maps for the months April, August and December  
314 for canyon ration (CR) 1.4, 1 and 0.5. It is clear that higher canyon ratios, which characterise a more compacted  
315 urban form, is more suitable for hot arid climate. This aligns with the results by Johansson's study of urban  
316 geometry in Fez, Morocco (2006) as well as the study of Ghardaia, Algeria (Toudert, & Mayer, 1997), where  
317 both researches suggest higher canyon ratios between buildings at the hot climates. The larger canyon ratio  
318 would allow less wind filtration, but it appears that the shading factor is more critical than the cooling by wind.

319 At the hottest point in the outdoor space, the UTCI temperature in CR0.5 is higher by 0.79°C than in  
320 CR1 (in April) and it is higher by 0.82°C in August, with no significant difference in December (Table 3 and  
321 Figure 14). This appears to be mainly to lack of shading by the buildings. At the coolest point of the outdoor  
322 space, which is the area close to the north façade of the lower block (Figure 14), the temperature difference is  
323 less significant between canyon ratio 0.5 and 1, with the maximum difference being 0.53°C in August. On the  
324 other hand, 0.5 CR is significantly higher in maximum temperature than 1.4 CR, with temperature difference as  
325 high as 1.25°C in August at the middle of the canyon and 0.53°C close to the northern façade (August). In  
326 December the canyon ratio seems to have no significant impact on the UTCI temperature. It is clear that the  
327 hotter the temperature, the more significant it is the impact of higher canyon ratio in reducing UTCI  
328 temperature.

329            Within canyon ratio 0.5, the temperature feels less by up to 3.62°C close to the northern façade than it  
330 does in the centre of the outdoor space, and less by up to 2.53°C than areas close to the southern façade (in  
331 April). This could be especially significant in allocating outdoor seating for cafes and restaurants, where in  
332 addition to other strategies the outdoor spaces can be brought to comfort in April and the similar months. In  
333 canyon ratio 1.4, the difference between the centre and the edges of the canyon is less prominent than in 0.5 CR,  
334 with 2.9°C difference in UTCI between the centre and the outdoor area close to the northern façade. While the  
335 impact of increasing the canyon ratio might not appear that significant in enhancing human comfort, its impact  
336 on reducing air conditioning peak demand is more apparent. With no additional strategies peak air condition  
337 demand can be reduced by 5% in a block when the canyon ratio is planned to be 1.4 instead of 0.5, and reduced  
338 by 3.2% between canyon ratios of 1 and 0.5 (figure.13). Any slight increase in peak load demand can have a  
339 considerable impact on the required equipment size for air condition, contributing to significantly higher  
340 equipment and operational costs. In Los Angeles, it was estimated that 5-10% increase in the peak energy  
341 demand caused by air condition cost the rate payers around 100 million dollars annually (Akbari, Pomerantz &  
342 Taha, 2001). The 100-million-dollar figure is from 2001 and do not account for inflation; hence the cost in 2018  
343 would be around 142 million according to the inflation calculator by Saving.org.

344 Table.3 CR impact on UTCI

Month	Max UTCI (Canyon centre)			Difference (°C)		Min UTCI (Close to N façade)			Difference (°C)	
	0.5	1	1.4	CR <sub>0.5</sub> -CR <sub>1</sub>	CR <sub>0.5</sub> -CR <sub>1.4</sub>	0.5	1	1.4	CR <sub>0.5</sub> -CR <sub>1</sub>	CR <sub>0.5</sub> -CR <sub>1.4</sub>
<b>April</b>	32.25	31.46	31.06	0.79	1.19	28.63	28.33	28.16	0.30	0.47
<b>August</b>	43.91	43.09	42.66	0.82	1.25	40.45	40.14	39.92	0.31	0.53
<b>December</b>	20.06	20.06	20.02	0.00	0.04	18.53	18.53	18.90	0.00	-0.37

345



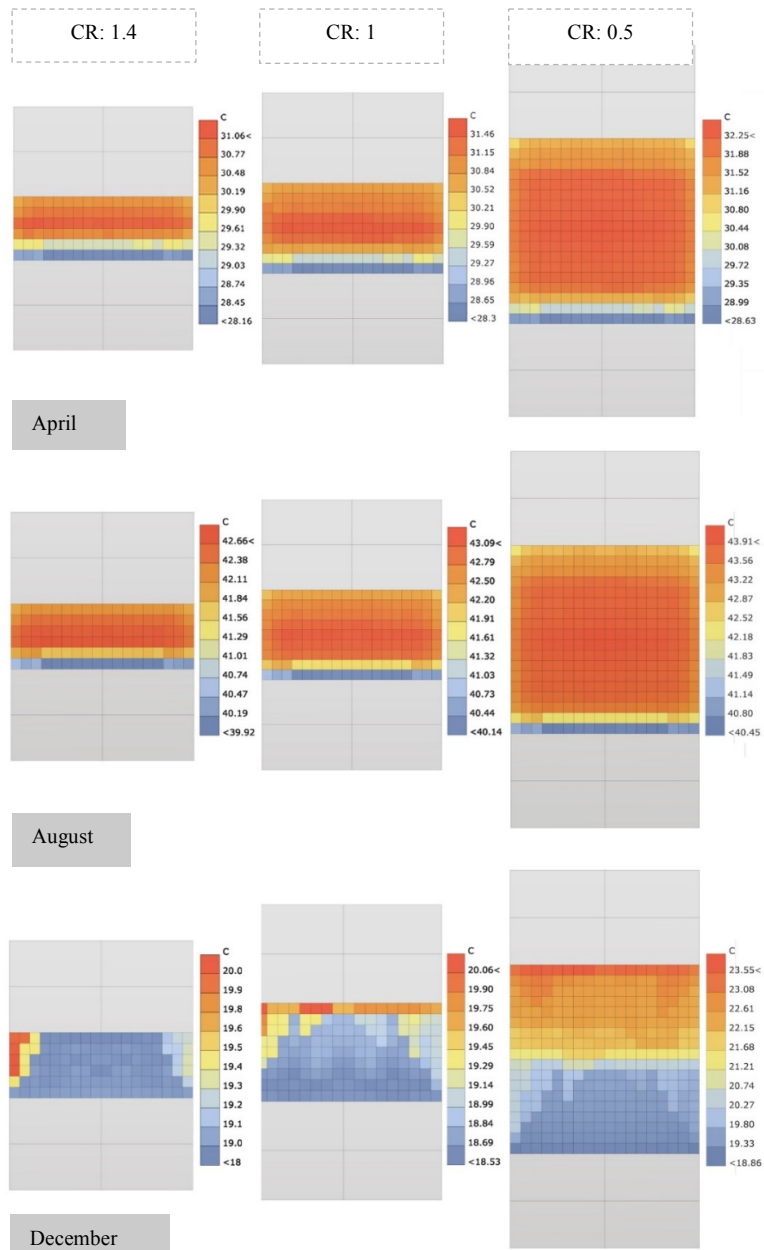


Fig.14 CR impact on UTCI test results

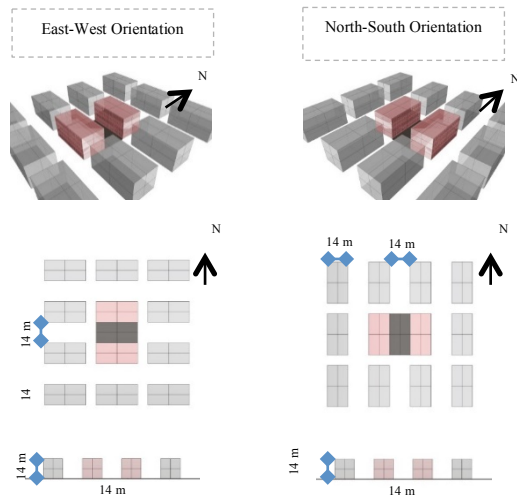
346

347 **4.2 The Impact of Street Orientation on Microclimate**

348 In order to examine which street orientation results in better outdoor comfort and energy consumption, testing of  
 349 the same canyon ration (1 CR) was conducted for two orientations: long canyon axis north-south and long  
 350 canyon axis east-west (Figure 15). Other model testing variables are similar to the testing of the impact of  
 351 canyon geometry (table.4).

<b>Canyon Ratio</b>	1
<b>Glazing percentage of the long façade</b>	30%
<b>Trees/ shading elements</b>	None
<b>Air-conditioning</b>	Ideal air flow
<b>Ground material</b>	Asphalt
<b>Buildings materials</b>	Refer to table.1
<b>Simulation height from the ground</b>	1.5 m

353



354

Fig.15 Street orientation test geometry

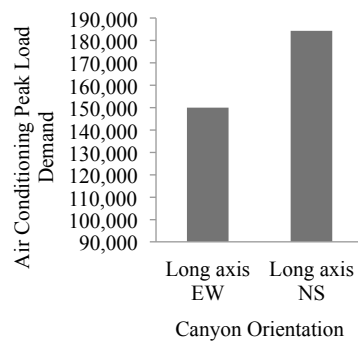


Fig.16 Air conditioning vs. street

355

356 The calculations showed that having the long axis of the canyon on the north-south orientation can lead  
 357 to reducing the UTCI temperature by 2.35°C in April and by 2.53°C in August at the central zone of the outdoor  
 358 space (Figure 17). In turn, in December the impact of canyon orientation seems less critical in comparison with  
 359 hotter months, which shows that E-W orientation has an opposite impact in winter, creating a generally warmer  
 360 environment by up to 1.35°C (Table 5). One explanation to the reduced impact in cooler months could be  
 361 attributed to the lower solar elevation angle in winter, especially from south, where the highest altitude angle in  
 362 December is 40° at noon, compared to 89° and 78° in April and August respectively (from Abu Dhabi weather  
 363 station .epw file). This leads to longer shading from by the southern building on the canyon in the E-W  
 364 orientation (figure 17). Meanwhile, the lower solar elevation angle in the N-W orientation is uninterrupted by  
 365 the buildings, which explains why the temperature in the N-W canyon increased slightly the in December.

366 However, the North-South orientation of the canyon long axis (and the buildings with it) had a negative  
 367 impact on the peak air-conditioning demand. The simulation shows that having the buildings longer façades

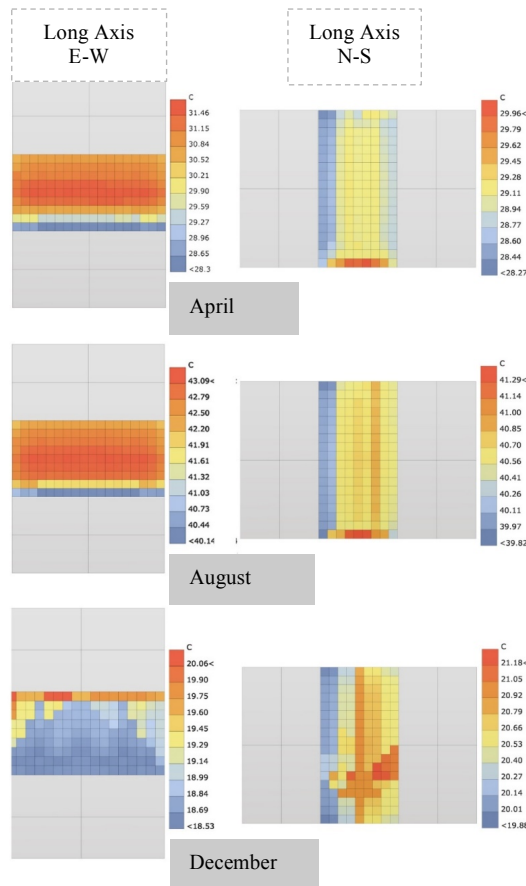
368 facing east and west (long axis on North- South) can increase air conditioning peak demand by around 23%  
 369 (figure 16). This result is mainly due to the fact that windows were only allocated on the longer facades in this  
 370 simulation, regardless of the orientation. So, in the case or the North-South canyon orientation, the main glazed  
 371 facades are facing East and West, which appears to cause more solar heat gain than having the main glazing on  
 372 the northern and southern facades. Therefore, while it is advisable to allocate the main outdoor areas on a North-  
 373 South street orientation, it is also critical to allocate the building longer axis on the East-West direction; mean-  
 374 ing that the building longer facades would face north and south (refer to urban strategies section).

375 As mentioned in the impact of canyon ratio section, the coolest areas in the outdoor space are closer to  
 376 the north façade in the E-W orientation. While in the N-S orientation the coolest areas are close to the Eastern  
 377 façade. To sum up, it seems that having the longer axis of the public space on the north-south axis leads to a  
 378 more comfortable urban environment in Al Ain/ Abu Dhabi climate; in April and August it reduces the UTCI  
 379 temperature, while in December it slightly increases it.

380 Table.5 Street Orientation impact on UTCI

Month orientation	Max UTCI		Difference (°C)	Min UTCI		Difference
	NS	EW	$CR_{EW}-CR_{NS}$	NS	EW	$CR_{EW}-CR_{NS}$
<b>April</b>	29.11	31.46	2.35	28.27	28.33	0.06
<b>August</b>	40.56	43.09	2.53	39.82	40.14	0.32
<b>December</b>	20.79	20.06	-0.73	19.88	18.53	-1.35

381



382

383 Fig.17 Street orientation impact on UTCI test results

384 **4.3 Case Study Application: Impact of Canyon Ratio and Street Orientation on Micro Climate in Al Ain**  
 385 **Town Square Neighborhood**

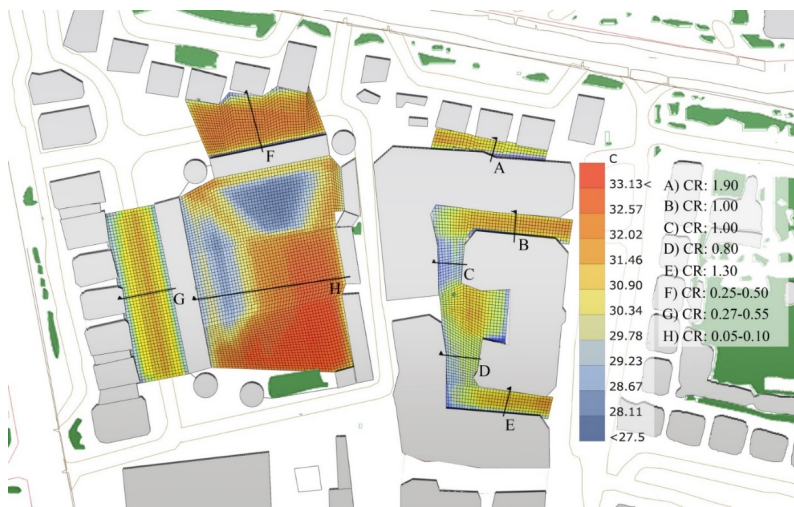
386 In this section, applying the simulation on the actual geometry of the town square was conducted for the April  
 387 month to test how representative the abstract scenarios are of the actual geometry. Subsequently, some strategies  
 388 were proposed in the urban strategies section to enhance the performance and liveability of the town square.

389 An overview of the map shows that canyons with higher ratio (Section A, Figure.19) are significantly  
 390 better performing than canyons with smaller ratio (section F), with difference of around 2-3°C UTCI at the  
 391 centre of the canyons. It also shows that at similar canyon ratios (Section B & C) N-S street orientation has a  
 392 better cooling effect than E-W orientation. In addition, even a wider canyon in the N-S orientation perform  
 393 better than a narrower street in the E-W orientation (section D and section A, and section D and E). The positive  
 394 impact of the N-S orientation is also clear between sections F and G, with difference of around 3°C UTCI  
 395 between the central areas.



396

397 Fig.18 Tensile structure in Al Ain Town Square (AlMawed, 2018).  
398



399

400 Fig.19 Application of UTCI micro-climate analysis on Al Ain Town Square Neighbourhood

401 Eastern and northern facades seem to be the coolest, and the large tensile structure that shades the  
402 outdoor space (Figure 18) seems to have very significant impact in cooling the outdoor space as it seems to  
403 make the outdoor space around 6°C UTCI cooler. These tensile structures are one of the defining characteristics  
404 of the square and take inspiration from the Bedouin tents that were one form of vernacular architecture in the  
405 region.

#### 406 4.4 The Impact of Shading by Vegetation on Microclimate

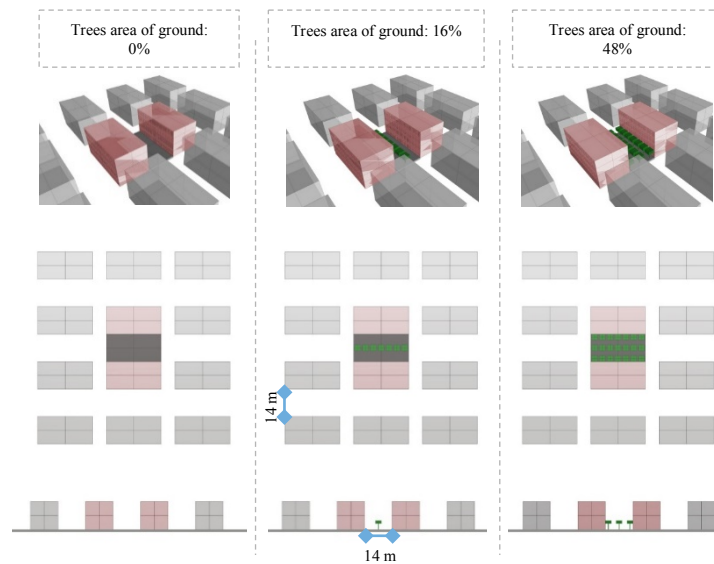
407 As discussed in the literature review section, many researchers agree that vegetation is one of the most impactful  
408 strategies in mitigating urban heat island and improve the microclimate. To test how much this strategy could  
409 improve the microclimate in Abu Dhabi/ Al Ain climate, simulations were conducted to compare green  
410 coverage of 16% and 48% (effective green coverage part) of the ground area, with the no shading case. The  
411 trees were assumed to have 3m clear height (6 m total height) and the effective shading volume is assumed to be  
412 27m<sup>2</sup> (3x3), based on *Prosopis Cineraria*, a native tree in UAE (ICRAF, 2009), with leaf area density (LAD)  
413 2.18 m<sup>2</sup>/m<sup>3</sup> (Perini et.al., 2017). In this paper only the shading impact of vegetation is studied. The

414 evapotranspiration impact was not included, where vegetation is treated as shading element only. Therefore, it is  
 415 expected that the actual influence of the green cover could be significantly higher than the simulated one.  
 416 Accordingly, other tree variables such as leaf temperature and leaf vapor flux were not studies. Figure 20  
 417 displays the three testing scenarios and Table 6 previews the constant variables in the test.

418 Table.6 Constant variables in the simulation of the impact of trees' shading on microclimate

<b>Street Orientation</b>	<b>East-West</b>
<b>Canyon Ratio</b>	1
<b>Glazing percentage of the long façade</b>	30%
<b>Air-conditioning</b>	Ideal air flow
<b>Ground material</b>	Asphalt
<b>Buildings materials</b>	Refer to table.1
<b>Simulation height from the ground</b>	1.5 m
<b>Leaf area density (LAD)</b>	2.18 m <sup>2</sup> /m <sup>3</sup>

419



420

421 Fig. 20 Urban vegetation test geometry

422 Figure 23 shows the impact of introducing green shading on improving microclimate. The simulation  
 423 shows that the temperature can feel up to 5°C less than without vegetation (Table 7). This result falls within the  
 424 same range reviewed by other studies. Table 7 also shows that the higher temperature, the more impactful  
 425 vegetation is. This agrees with Perini and Magliocco's (2014) observation about the increased impact of  
 426 vegetation the hotter the temperatures. It should be pointed out that the literature reviewed measured the impact  
 427 on air temperature, while this study uses UTCI temperature. However, the review can be used as an indicator  
 428 that the simulated results are reasonable.

429 Table.7 Shading by vegetation impact on UTCI

Month	UTCI (maximum)			Difference (°C)		UTCI (minimum)			Difference (°C)	
	0%	16%	48%	Veg <sub>0%</sub> - Veg <sub>16%</sub>	Veg <sub>0%</sub> - Veg <sub>48%</sub>	0%	16%	48%	Veg <sub>0%</sub> - Veg <sub>16%</sub>	Veg <sub>0%</sub> - Veg <sub>48%</sub>
<b>April</b>	31.46	30.65	30.3	0.81	1.16	28.33	27.17	26.48	1.16	1.85
<b>August</b>	43.09	42.39	41.85	0.70	1.24	40.14	38.81	38.06	1.33	2.08
<b>December</b>	20.06	20.06	19.62	0.00	0.44	18.53	18.39	18.32	0.14	0.21

430

431 To further illustrate how much shading by greenery can add to microclimate, Figure 21 and 22 present how  
432 much each tested shading surface percentage can impact the felt temperature (UTCI). For Example, in April 0%  
433 shading, 78% of the total tested outdoor area feels like above 30 °C, while 22% of the total area feels between  
434 28 and 30°C. However, when 48% vegetation is introduced, less than 15% of the total outdoor space feels hotter  
435 than 30°C, while quarter of the space feels between 28 -30°C and more than 60% of the total area have a mild  
436 heat stress, with a UTCI temperature range of 26 to 28°C. Figure 21 could also provide an approximate method  
437 to interpolate the expected impact of other green-cover percentages for April, and possibly the months with  
438 similar climatic characteristics (May, October and November). It could be used as an approximation method to  
439 roughly estimate how much shading surface should be used. For example, a 32% increase in vegetation surface  
440 would roughly make 40% of the outdoor space in the <28°C UTCI range, and decrease the outdoor area that  
441 feels 30°C> from 78% (at 0% shading) to 40%. Meanwhile, Figure 22 can be used to estimate the impact of  
442 vegetation in mitigating the intensity of heat stress in June, July, August and September.

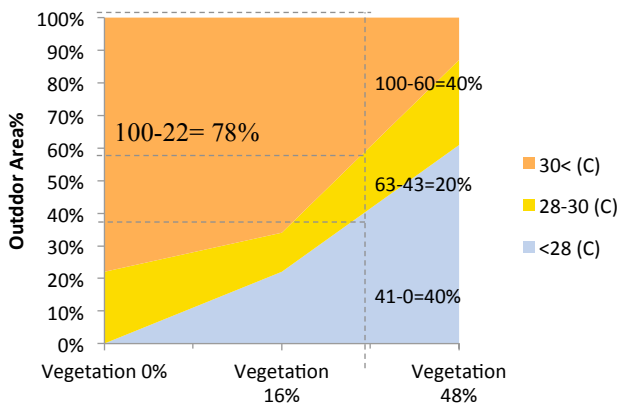


Fig.21 Shading surface% impact in April

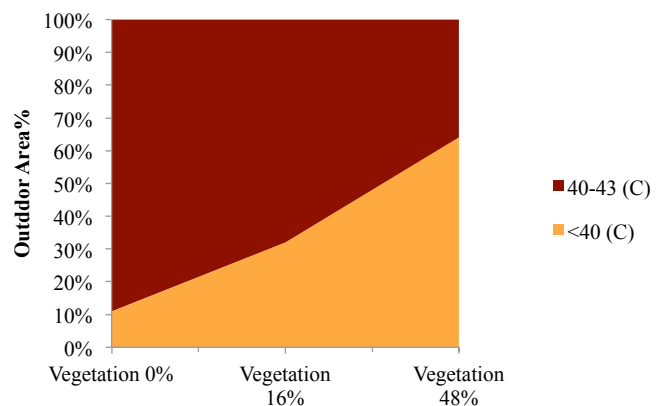
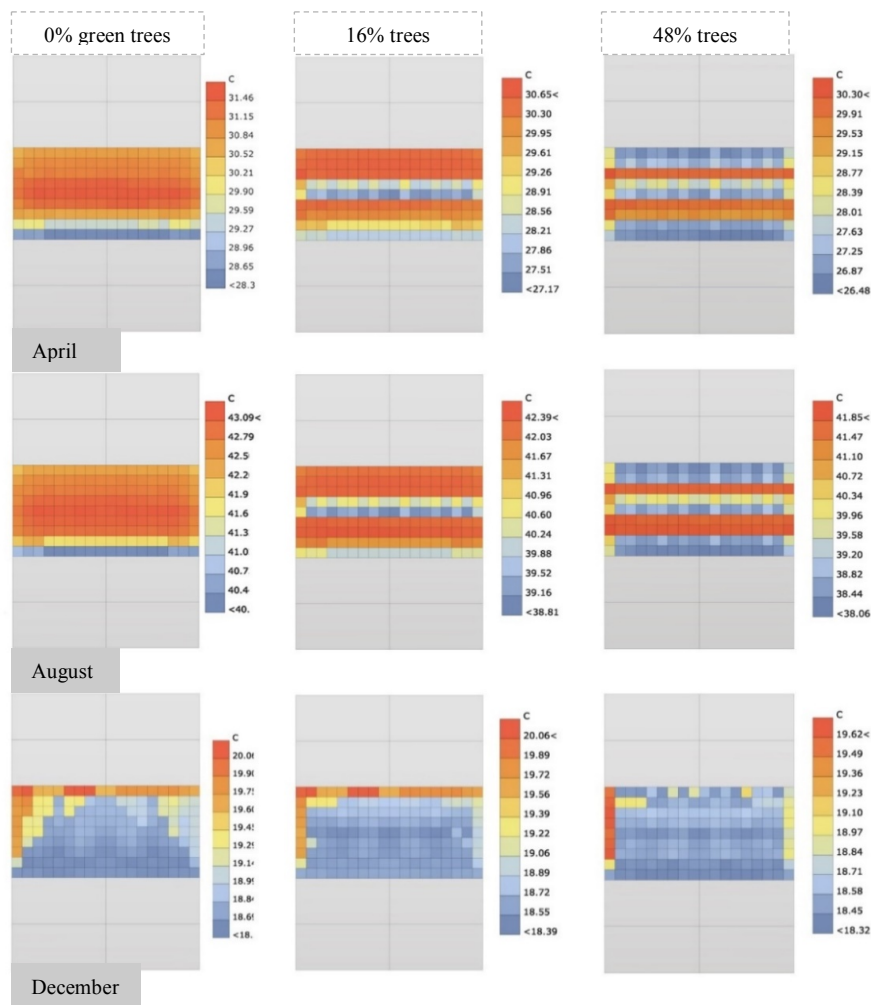


Fig.22 Shading surface% impact in August

443

444 On the other hand, the simulation shows no significant change in peak air conditioning demand. It  
445 appears that there is barely 1% reduction in peak demand between 0% (150 kW) and 48% (148.5 kW)  
446 vegetation, and around 0.15% reduction between 0% and 16% vegetation. These results contrasts with Akbari's  
447 book (2009) which shows a much higher potential for decreasing peak air conditioning demand. His work shows  
448 that in Phoenix (one of the closest examples to UAE climate characteristics), 12% to 17% saving in annual  
449 energy can be achieved through increasing the green cover by 10% to 25%. The reason for such variation is that

450 Akbari's study is conducted on one floor houses while this study is performed on a four-story building with a  
 451 significantly higher cooling demand, and the shading effect of the trees mainly impacts the ground floor. This  
 452 makes the impact of shading on cooling demand in this study not very significant when compared to the overall  
 453 energy demand of the multi-story building. Moreover, the trees are positioned in shading position in Akbari  
 454 study, while in this research the trees are shading one side of each building that form the outdoor envelope  
 455 (Figure 20) since the main focus of the research is the impact on outdoor areas. This leaves the southern façade  
 456 of one of the buildings nonshaded. Additionally, Akbari (2009) has included the evapotranspiration impact,  
 457 which can significantly contribute to reducing cooling demand. He argues that in well-insulated buildings, the  
 458 shading effect becomes less significant than the evapotranspiration effect; that out of the 17% cooling reduction  
 459 in a well-insulated house in Phoenix, 10% reduction is caused by evapotranspiration and 7% by tree shading. He  
 460 argues that in older, less insulated houses the tree shading effect becomes more important than the  
 461 evapotranspiration one. Evidence of this can be seen in an older study by Simpson and McPherson (1998),  
 462 where they simulated the impact of vegetation shading by planting three trees per house on 254 houses in  
 463 California (around 25% increase in green cover), and around 7.1% reductions in cooling demand were achieved.

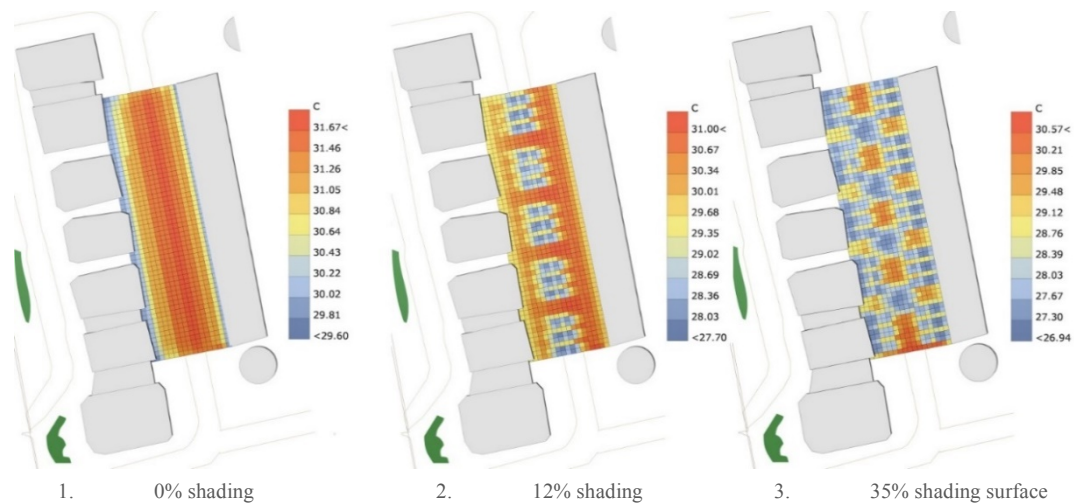




465 Fig.23 Shading by vegetation impact on UTCI test results

466 **4.5 Case Study Application: Impact of Vegetation on Micro Climate, in Al Ain Town Square Neighborhood**

467 One region of the neighborhood has been selected to apply the impact of vegetation on. Figure 24 displays the  
468 comfort map for section G, with no shading surface (A), 12% shading surface (B) and 35% shading surface (C).  
469 Under the shading surface the UTCI temperature can be lower by around 5°C compared with no shading,  
470 making 50% of the outdoor area in the 26-28 °C (in the case of C, which is defined by Outdoor Comfort  
471 Calculator in Grasshopper as comfortable for a short-time temperature). Moreover, according to Al-Shaali  
472 (2013) this range can be brought to comfort through accelerated wind speed. He suggests that 27-30°C  
473 temperatures can be made to become completely comfortable through accelerated wind speed (for UAE  
474 climate).



476 Fig.24 Application on Al Ain Town Square Neighbourhood

477 **4.6 The Impact of Wind Speed on UTCI**

478 Wind dynamics around buildings forms complex flow patterns that could have contradictory impacts, such as  
479 acceleration and buffering of wind speed (Ishugah, Wang & Kiplagat, 2014). Some of these patterns of  
480 acceleration include corner jetting and downwash (Heywood, 2015). A compact urban form has the advantage  
481 of improving microclimate through shading, but it can also present a negative impact by blocking wind  
482 circulation. The literature review indicates that in hotter climates, compact urban forms are preferable over  
483 sprawled forms (smaller canyon ratio) even though the compact form compromise the ventilation effect. This  
484 indicates that wind ventilation should be integrated without compromising the shading effect.

485 Analysis through climate consultant of Al Ain/ Abu Dhabi climate showed that the prevalent wind  
486 direction throughout the year is from NW, with a speed ranging from 2 to 6 m/s (data in brief, figure 4).

487 Accordingly, a north-western wind of 2 m/s, 4 m/s and 6 m/s had been simulated (using Flow Design software)  
488 for Al Ain town square neighbourhood, to first observe the wind circulation in the scheme, then observe the  
489 impact of opening the ground floor of some of the buildings in the north western direction. The ground floor  
490 openings would enhance the ventilation in the outdoor areas without compromising the shading factor.

491 The applied wind direction was assumed to be un-buffered by other buildings outside the  
492 neighbourhood, where there are 50-55 m main streets separating the town square neighbourhood from the  
493 surrounding ones (refer to Figure 8). Moreover, only the prominent wind direction from the north west was  
494 considered. Additionally, UTCI comfort maps using the changed geometry were not generated due to time  
495 limitation. Figure 25 shows the existing geometry, while Figure 26 shows the changes made to allow more air  
496 circulation in the scheme. The wind simulation in Flow Design shows better ventilation with the edited  
497 geometry (Figure 27). When 2 m/s was applied, the original scheme showed very minimal wind circulation,  
498 which increased to become between 1 to 2 m/s with the new opening. Similarly, with 4 m/s initial wind velocity  
499 the air circulation in the area had been enhanced and reached a speed of 2.7 m/s. Meanwhile with 6 m/s, the  
500 wind speed in the scheme was as high as 6 m/s.

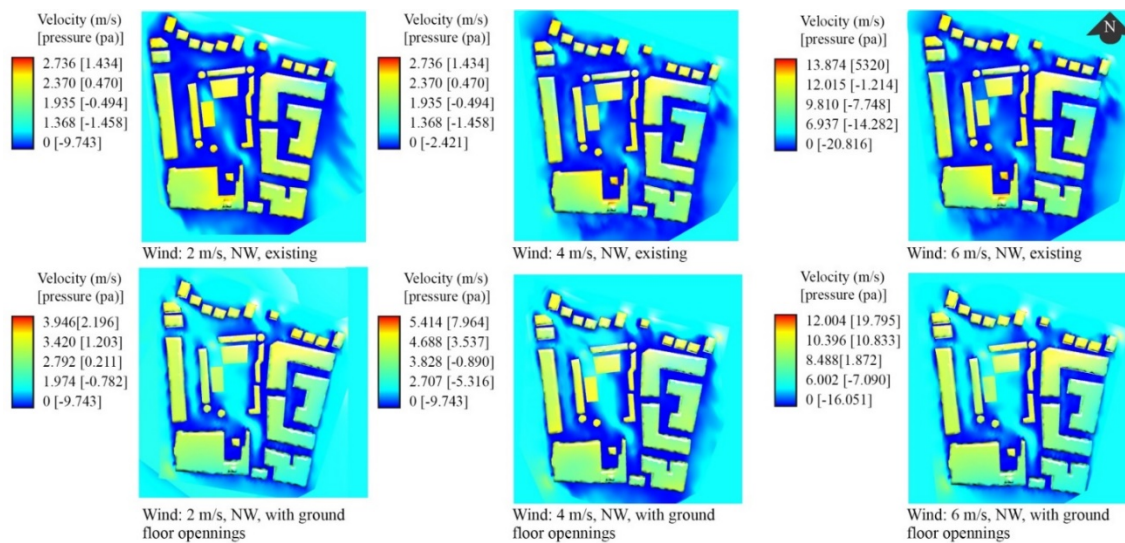


Fig.25 Existing geometry, very little air passages on pedestrian level



Fig.26 Edited geometry, some ground floors in NW turned to outdoor areas creating wind passages and increases the permeability to the

501  
502 Meanwhile, Grasshopper (with Ladybug Plug-in, Outdoor Comfort Calculator) was used to record the  
503 possible impact changing wind speeds would have on how the temperature feels (UTCI), at a constant relative  
504 humidity of 50%, 1 clo and 1 MET (Figure 28). Wind speeds from 0 to 6 m/s were applied to temperature from  
505 26 to 32°C, which is the moderate heat stress range that is targeted to be brought to comfort as discussed  
506 previously. This range is mainly in April, May, October and November. In the Impact of Shading Surfaces  
507 section (4.5), simulations show that it is possible to bring more than half the outdoor space to the temperature  
508 range 26-28°C through a shading 35% of the outdoor area (considering all the other constant variables), this  
509 indicates that the area could be brought completely to comfort through accelerating the wind circulation in the



511

512 Fig.27 Wind circulation in the scheme for initial applied wind speed of 2 m/s, 4 m/s and 6 m/s from north west.  
 513 It is clear that the edited geometry provides better wind ventilation for the scheme.

514 For example, if air temperature is 28 °C, a wind speed of 2.7 m/s would cause UTCI to be:

515 ○  $y_{28} = -0.8853(2.7 \text{ m/s}) + 28.776$

516 ○  $y_{28} = 26.39 \text{ °C UTCI}$ .

517 For the same air temperature and a wind speed of 6 m/s:

518 ○  $y_{28} = -0.8853(6 \text{ m/s}) + 28.776 = 23.46 \text{ °C UTCI}$ .

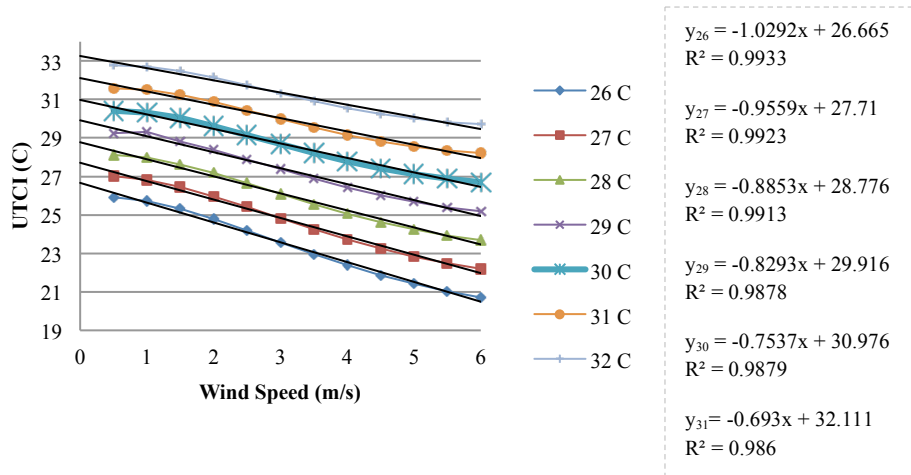
519 If air temperature 32 °C, and wind speed is 3.6 m/s:

520 ○  $y_{32} = -0.6331(3.6) + 33.259$

521  $y_{32} = 30.97 \text{ °C UTCI}$ , while a wind speed of 6 m/s would result in felt temperature of 29.46 °C.

522 It is noticed from the line graph that the lower the temperature, the larger the impact of wind speed  
 523 (steeper slope for  $y_{26}$  than  $y_{32}$ ). It appears that the UTCI equations developed by the International Society of  
 524 Biometeorology, which this simulation of UTCI is based on, indicates that higher temperatures the increased  
 525 wind speed becomes less effective in reducing the human perception of heat stress. These UTCI equations  
 526 involve meteorological as well as non-meteorological variables relating to human comfort as discussed in  
 527 literature review. Therefore, further research in assessing the equations that calculate UTCI need to be made for  
 528 more accurate explanation of the decreased wind speed impact on UTCI at higher temperatures.

529 The results are very comparable to what was found by Taleb & Abu-Hijleh (2013). Their study,  
 530 conducted in Dubai using ENVI-Met software, found that wind speed of 3.6 m/s could reduce an initial  
 531 temperature of 32°C to 29.06°C ± 2.72 (the volume orthogonal configuration, June). The slight differences could  
 532 be attributed to the different simulation software's calculation methods.



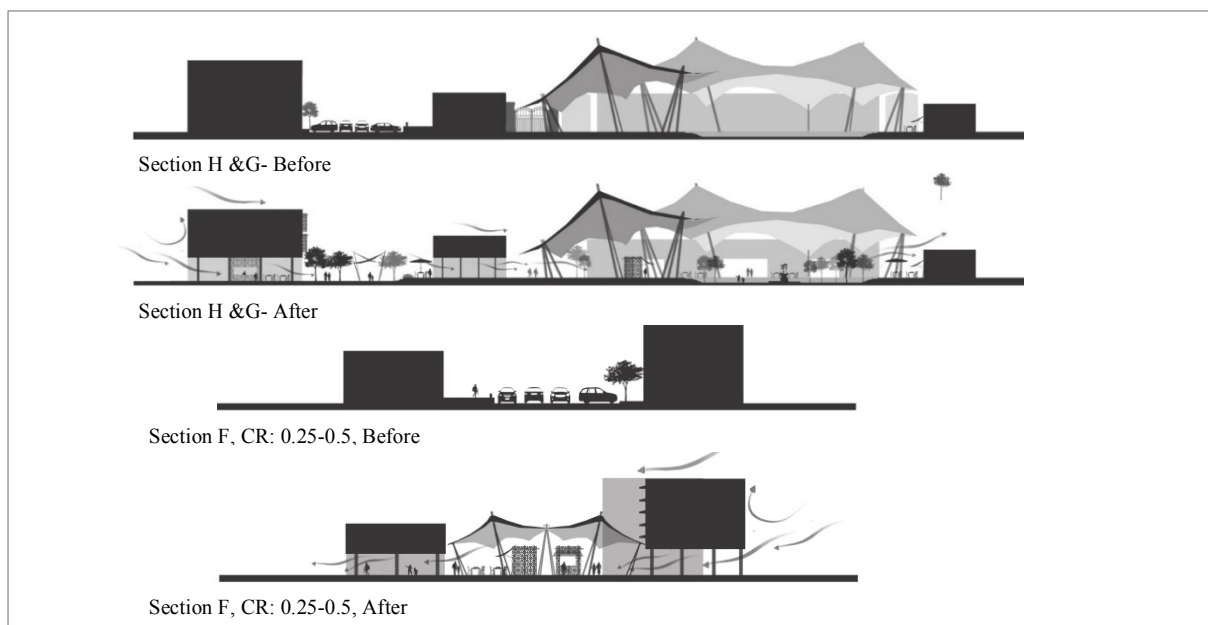
533

534 Fig.28 The impact of wind speed on how the temperature feels at 50% relative humidity, where x is wind speed  
 535 and y is the resultant UTCI value. Data obtained from outdoor comfort calculator, grasshopper.

536 **5. Urban Strategies**

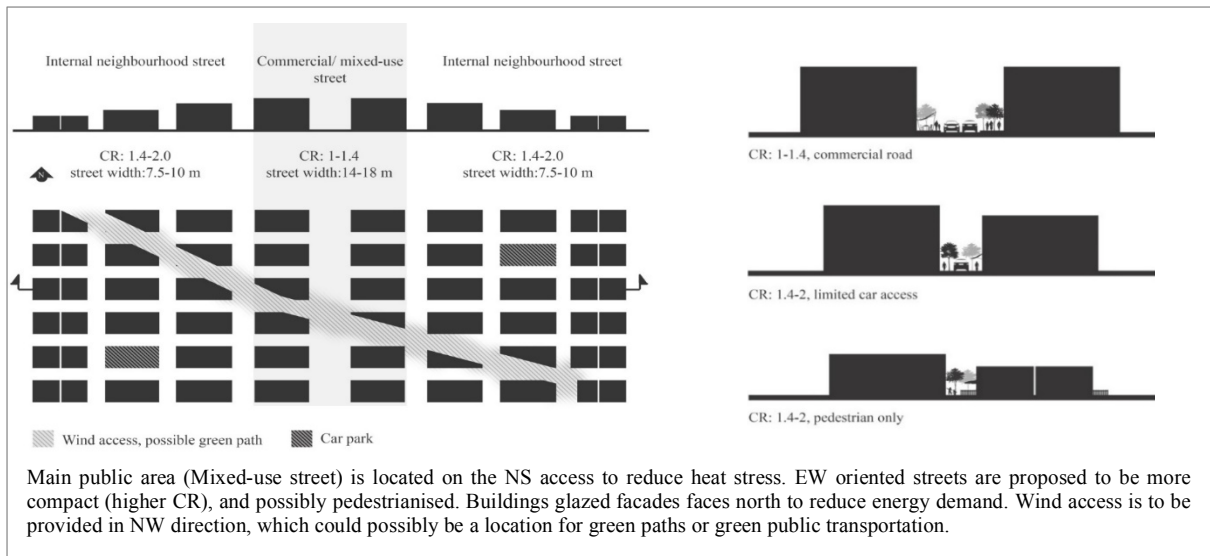
537 Based on the previous tests, Figure 29 displays some recommendation/ strategies that can be used to enhance the  
 538 microclimate comfort and vitality of Al Ain town square. Meanwhile, Figure 30 displays some recommended  
 539 strategies for a new neighbourhood block design for Al Ain/ Abu Dhabi climate based on orientation, canyon  
 540 ratio and wind circulation. Figure 31, in turn, shows guiding strategies for urban vegetation considering  
 541 buildings height and functions.

542



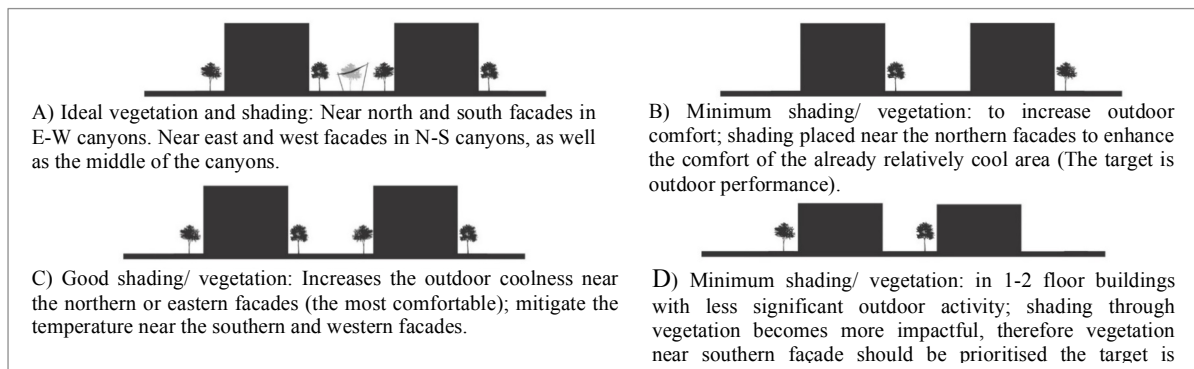
543

544 Fig.29 Strategies for Al Ain town square



545

546 Fig.30 General strategies for new communities in UAE climatic conditions



547

548 Fig.31 General strategies for shading by vegetation

## 549 6. Conclusion

550 The present study was designed to determine the impact of urban design strategies on microclimate in hot arid  
 551 climatic conditions. The study focuses on assessing the impact of canyon ratio, outdoor orientation and wind  
 552 speed in Al Ain city. Higher canyon ratios appear to be better performing in hot arid climate, where the shading  
 553 impact of the compact urban form seems to be more significant than the wind circulation impact that can be  
 554 compromised with compact forms. A canyon ration (CR) no less than 1 is recommended, with an overall range  
 555 from 1 to 2 CR depending on the street hierarchy. This study has found that NS orientation of outdoor public  
 556 spaces is significantly better performing in terms of microclimate comfort (2-3°C cooler) with the coolest zones  
 557 being next to the northern or eastern facades.

558 Moreover, it was found that shading surfaces/ vegetation shading can contribute to reducing UTCI  
 559 temperature by around 4-5°C in April and August in UAE climate, and higher impact was recorded at the hotter

560 seasons. Another finding to emerge from this study is that creating “openings” in the prominent wind direction  
561 can contribute significantly to ventilation in the outdoor area without compromising the shading effect, which  
562 can dramatically reduce UTCI temperature from the moderate heat stress range (26-32 °C) to comfort or close to  
563 comfort. The resultant interpolated graph (Figure 28) can possibly allow to predict the expected felt temperature  
564 at a certain wind speed (0 to 6 m/s) and air temperature range of 26-32 °C.

565         These findings can have significant implications for advising decision making in urban planning and  
566 urban design in UAE, as well as in similar hot arid environmental contexts. They can be applied in both new  
567 developments and in strategies for improving the existing urban fabric, which could contribute to more  
568 liveability and vitality in outdoor areas. Finally, the produced estimation methods of the impact of shading  
569 surfaces and wind speed on outdoor comfort can possibly help designers in evaluating the impact of their urban  
570 design strategies in similar climates.

571         A limitation of this study is that EnergyPlus uses a simple wind profile that do not account for  
572 obstructions. Computational fluid dynamics (CFD) component can be used for higher accuracy of the results,  
573 which was not used in this study due to time and resource limitations. Moreover, the study did not evaluate the  
574 impact of evapotranspiration in trees, and considered only their shading effect, which indicates that the actual  
575 cooling effect is expected to be even higher. Finally, the results of wind simulation using Flow Design are  
576 valuable in showing the general behavior of wind in a scheme in the initial stages of design, however, more  
577 advanced software (such as ENVI-Met) can give more accurate results for the advanced stages of design.

578         Additional field research should be performed to validate the accuracy of UTCI simulations in hot arid contexts  
579 experimentally. While UTCI calculations has been validated experimentally in sub-tropical climate of southern  
580 Brazil, as well as in Canada and Korea, similar study can be performed in UAE context to test the local  
581 subjective thermal comfort in the region.

582         A greater focus on how to accelerate wind in urban areas in hot arid climates through urban structures  
583 could produce interesting findings on how to bring the moderate heat stress periods of the year to comfort,  
584 which would also reduce the intensity of high heat stress months. Moreover, a further study could assess the  
585 evapotranspiration impact of vegetation in UAE climate. Finally, more research on the economical implication  
586 of reducing peak air conditioning demand in UAE could help this research to be more impactful to decision  
587 makers in urban planning.

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